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OR FLS,

## A FORTRAN CRYSTALLOGRAPHIC LEAST-SQUARES PROGRAM

W. R. Busing  
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OR FLS,

A FORTRAN CRYSTALLOGRAPHIC LEAST-SQUARES PROGRAM

by

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Chemistry Division and Mathematics Division

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#### ABSTRACT

This report describes a computer program to perform the least-squares refinement of crystal structure parameters based on x-ray or neutron diffraction measurements. The program is written mostly in the Fortran language to facilitate modification and to permit its use on various machines. Detailed instructions for its use are included, and the required card decks may be obtained from the authors.

## INTRODUCTION

This report describes a computer program to perform the least-squares refinement of crystal structure parameters based on x-ray or neutron diffraction measurements. Detailed instructions for its use are included, and the required card decks may be obtained from the authors.

The program performs successive cycles of refinement using the full matrix of the normal equations. The parameters which may be adjusted include several scale factors, an over-all temperature factor coefficient, the neutron scattering factors, individual atom multipliers, atomic coordinates, and isotropic or anisotropic individual atom temperature factor coefficients. The parameters to be varied may be specified arbitrarily, and structures of any symmetry may be accommodated. The refinement may be based either on the structure factors or their squares, and the observations may be weighted individually, or the use of unit weights may be specified.

The program is mathematically similar to an earlier version, OR XLS (W. R. Busing and H. A. Levy, "A Crystallographic Least Squares Refinement Program for the IBM 704," ORNL-CF 59-4-37, 1959). A basic difference is that the present program is not segmented and does not use magnetic tape for intermediate storage. This implies that a 32k core memory will be required for most problems. A means of expanding the storage capacity with magnetic tape is

mentioned briefly in a later section. Provision is made to transfer parameters from one job to the next by means of magnetic tape or punched cards.

The present program is derived from a general least-squares program (W. R. Busing and H. A. Levy, "OR GLS, A General Fortran Least Squares Program," ORNL-TM-271, 1962), and programmers contemplating extensive changes should consider starting with that basic program.

In order to facilitate modification of the program and to permit its use on various machines, OR FLS has been written in the Fortran language except for the matrix inverter which is in FAP suitable for the IBM 704, 709, or 7090. A test problem is provided to serve as an example and to aid in checking the program at other installations.

#### GENERAL DESCRIPTION

It is expected that the Fortran listing and the glossary of symbols which are provided will serve as a complete description of the program. The form of the input is described in detail in a separate section, and an example of such input, together with the corresponding output, is also given. This section, therefore, is intended to serve only as a summary of the method.

Because the present routine is a modification of the general least-squares program, OR GLS, it was convenient to divide it into several subprograms. The main program performs the basic operations associated with the least-squares

refinement, while subroutine PRELIM serves to read the control information and parameters which define the trial crystal structure. Subroutine CALC computes the scaled structure factors or their squares and the derivatives of these quantities with respect to the trial parameters, and subroutine TEST determines whether the adjusted temperature factor coefficients are positive-definite.

In the calculation of the structure factors and their derivatives it is useful to distinguish the different types of parameters such as scale factors, coordinates, and temperature factor coefficients and to store them in separate arrays. For the least-squares adjustment procedure, however, it is more convenient to store all the parameters in a single array. To achieve both of these objectives the program uses duplicate storage arrays for the crystal structure parameters, and subroutine PTOSB is provided to copy them from the array P to the various storage locations SC, TO, SF, AI, XYZ, and BETA. Subroutine SBTOP performs the reverse information transfer and is also used to execute an analogous operation with the calculated derivatives.

The sequence of operations begins with the reading of all the input data. This is performed partly by the main program and partly by subroutine PRELIM. Most of the items read are immediately put out by the program to aid in diagnosing difficulties.

If the control card indicates that isotropic temperature

factor coefficients,  $T_i$ , are to be converted to anisotropic form, subroutine PRELIM computes for each atom

$$\beta_{11i} = T_i a^{*2}/4,$$

$$\beta_{12i} = T_i a^* b^* \cos\gamma^*/4,$$

etc.

Here the  $\beta$ 's are the anisotropic temperature factor coefficients defined in the next section, and  $a^*$ ,  $b^*$ , ...,  $\gamma^*$  are the reciprocal cell parameters. The program then proceeds as though anisotropic coefficients had been read.

For each cycle the matrix and vector of the normal equations are stored by computing the contributions of one observation at a time. For this purpose subroutine CALC is entered once for each reflection to obtain YC, the calculated absolute value of the scaled structure factor or its square. CALC also stores in the array DC the derivatives of YC with respect to all parameters, P, whether they are to be varied or not. The expressions for these quantities are summarized in the following table, in which F is the magnitude of the structure factor,  $s_q$  is the scale factor,  $T_o$  is the over-all temperature factor coefficient,  $\rho$  is  $\sin^2\theta/\lambda^2$ , A and B are the real and imaginary components of the structure factor, and p is any individual atom parameter.

	Centrosymmetric with origin at symmetry center	Non-centrosymmetric
$(s_q F)$	$2s_q \exp(-T_O \rho)  A $	$s_q \exp(-T_O \rho) (A^2 + B^2)^{1/2}$
$\partial(s_q F)/\partial s_q$	$(s_q F)/s_q$	$(s_q F)/s_q$
$\partial(s_q F)/\partial T_O$	$-\rho(s_q F)$	$-\rho(s_q F)$
$\partial(s_q F)/\partial p$	$2s_q \exp(-T_O \rho) (\partial  A /\partial p)$	$s_q \exp(-T_O \rho) (A^2 + B^2)^{-1/2} \cdot [A(\partial A/\partial p) + B(\partial B/\partial p)]$
$(s_q F)^2$	$4s_q^2 \exp(-2T_O \rho) A^2$	$s_q^2 \exp(-2T_O \rho) (A^2 + B^2)$
$\partial(s_q F)^2/\partial s_q$	$2(s_q F)^2/s_q$	$2(s_q F)^2/s_q$
$\partial(s_q F)^2/\partial T_O$	$-2\rho(s_q F)^2$	$-2\rho(s_q F)^2$
$\partial(s_q F)^2/\partial p$	$8s_q^2 \exp(-2T_O \rho) A(\partial A/\partial p)$	$2s_q^2 \exp(-2T_O \rho) \cdot [A(\partial A/\partial p) + B(\partial B/\partial p)]$

The expressions for A and B and their derivatives are summarized in the following table. Here the subscripts i and j refer to the various atoms in the asymmetric unit and to the different equivalent positions, respectively.  $T_i$ ,  $f_i$ , and  $a_i$  are the isotropic temperature factor coefficient, scattering factor, and scattering factor multiplier, respectively, for atom i. The terms  $\cos_{ij}$ ,  $\sin_{ij}$ , and  $\exp_{ij}$  are the trigonometric contributions and the anisotropic temperature factor of atom i in equivalent position j. The expressions  $h_j$  and  $(2hk)_j$  are representative of the transformed indices and index products. These terms are discussed in detail in the next section.

	Isotropic temperature factor	Anisotropic temperature factor
A	$\sum_i f_i a_i \exp(-T_i \rho) \sum_j \cos_{ij}$	$\sum_i f_i a_i \sum_j \exp_{ij} \cos_{ij}$
B	$\sum_i f_i a_i \exp(-T_i \rho) \sum_j \sin_{ij}$	$\sum_i f_i a_i \sum_j \exp_{ij} \sin_{ij}$
$\partial A / \partial f_i$	$a_i \exp(-T_i \rho) \sum_j \cos_{ij}$	$a_i \sum_j \exp_{ij} \cos_{ij}$
$\partial B / \partial f_i$	$a_i \exp(-T_i \rho) \sum_j \sin_{ij}$	$a_i \sum_j \exp_{ij} \sin_{ij}$
$\partial A / \partial a_i$	$f_i \exp(-T_i \rho) \sum_j \cos_{ij}$	$f_i \sum_j \exp_{ij} \cos_{ij}$
$\partial B / \partial a_i$	$f_i \exp(-T_i \rho) \sum_j \sin_{ij}$	$f_i \sum_j \exp_{ij} \sin_{ij}$
$\partial A / \partial T_i$	$-\rho f_i a_i \exp(-T_i \rho) \sum_j \cos_{ij}$	-----
$\partial B / \partial T_i$	$-\rho f_i a_i \exp(-T_i \rho) \sum_j \sin_{ij}$	-----
$\partial A / \partial x_i$	$-2\pi f_i a_i \exp(-T_i \rho) \sum_j h_j \sin_{ij}$	$-2\pi f_i a_i \sum_j h_j \exp_{ij} \sin_{ij}$
$\partial B / \partial x_i$	$2\pi f_i a_i \exp(-T_i \rho) \sum_j h_j \cos_{ij}$	$2\pi f_i a_i \sum_j h_j \exp_{ij} \cos_{ij}$
$\partial A / \partial B_{12i}$	-----	$-f_i a_i \sum_j (2hk) \exp_{ij} \cos_{ij}$
$\partial B / \partial \beta_{12i}$	-----	$-f_i a_i \sum_j (2hk) \exp_{ij} \sin_{ij}$

The program does the computation for each reflection in three steps. First the sums over j are accumulated. These are then converted to the derivatives of A and B with respect to the atomic parameters, and A and B are obtained. Finally, the scaled structure factor or its square and the derivatives of this quantity are computed.

Upon return from subroutine CALC, a line of output comparing the observation with its calculated value is put out. The term  $(\text{SQRTW} * \text{DV}(J)) * (\text{SQRTW} * \text{DV}(K))$  is then added to  $\text{AM}(JK)$ , the J,Kth element of the matrix, where SQRTW is the square root of the weight of the observation. The contribution to the vector element  $\text{V}(J)$  is  $(\text{SQRTW} * \text{DV}(J)) * (\text{SQRTW} * (\text{Y}_0 - \text{Y}_C))$ , and that to the agreement factor SIG is  $(\text{SQRTW} * (\text{Y}_0 - \text{Y}_C))^{**2}$ . Here YO is used as an abbreviation for  $\text{Y}_0(I)$ , the Ith observed value of  $|F|$  or  $F^2$ .

The sums involved in the following unweighted and weighted R factors are accumulated both for all observations and for non-zero observations.

	Refining on $ F $	Refining on $F^2$
R	$\Sigma  F_O - s_q F  / \Sigma  F_O $	$\Sigma  F_O^2 - (s_q F)^2  / \Sigma  F_O^2 $
Weighted R	$\sqrt{\sum w(F_O - s_q F)^2} / \sqrt{\sum w F_O^2}$	$\sqrt{\sum w(F_O^2 - (s_q F)^2)^2} / \sqrt{\sum w(F_O^2)^2}$

The calculation of YC and its derivatives is repeated until the contributions from all the observations have been obtained. At this point an agreement factor, the standard error of an observation of unit weight,  $\text{SQRTF(SIG/(NO-NV))}$ , is computed and put out together with the R factors.

The storage scheme used for the matrix AM is described in the glossary. To make efficient use of memory space,

only the upper triangular part of this symmetric matrix is stored. Furthermore, to conform to the requirements of the existing matrix inverter, SMI, the matrix is stored forward in core or backward in the normal Fortran indexing system.

Before the matrix is inverted it is tested for zero diagonal elements, which would indicate a singular matrix with one or more zero row-columns. This would be the result if the derivatives with respect to the corresponding parameters were zero for all observations. A singular matrix due to the attempt to vary sets of parameters with one or more redundancies will be found in the course of the inversion. In case of either type of singularity, the job is terminated with the appropriate comment.

The matrix inversion procedure is described in detail elsewhere (W. R. Busing and H. A. Levy, "A Procedure for Inverting Large Symmetric Matrices," Comm. ACM (Aug. 1962) 5 445-446). It involves the diagonalization of the matrix by a series of congruent transformations, inversion by taking reciprocals of the diagonal elements, and a sequence of reverse transformations. Upon completion of the process the inverse matrix has replaced the original one in the array AM.

The vector is then multiplied by the inverse matrix to obtain the parameter changes, PD. An estimated new value of the agreement factor SIG is obtained by subtracting from it  $\text{PD}(I)*V(I)$  summed over the NV variables, and a revised  $\text{SQRTF}(\text{SIG}/(\text{NO}-\text{NV}))$  is computed. The entire list of parameters is then put out showing the changes which were made and the

estimated standard errors associated with these variables.

The latter are computed as SQRTF(DIAG(J)\*SIG/(NO-NV)), where DIAG is an array of the diagonal elements of the inverse matrix. It should be noted that these estimates are approximately correct if the refinement is converging but may be grossly incorrect if the calculation is diverging.

The program then calls subroutine TEST to examine the new temperature factor coefficients. If the over-all temperature factor  $T_o$  is not zero, it is added to the individual atom temperature factors so that  $T'_i = T_i + T_o$  for isotropic temperature factors or

$$\begin{aligned}\beta'_{11} &= \beta_{11} + T_o a^2/4, \\ \beta'_{12} &= \beta_{12} + T_o a*b*\cos\gamma*/4, \\ &\text{etc.,}\end{aligned}$$

for anisotropic temperature factors.  $T_o$  is then set to zero. These operations are performed so that the temperature factor coefficients may be tested for positive-definite form in the following way. For isotropic temperature factors:

$$T_i \geq 0.$$

For anisotropic temperature factors:

$$\begin{aligned}\beta_{11} &\geq 0, \quad \beta_{22} \geq 0, \quad \beta_{33} \geq 0, \\ \left| \begin{array}{cc} \beta_{22} & \beta_{23} \\ \beta_{23} & \beta_{33} \end{array} \right| &\geq 0, \quad \left| \begin{array}{cc} \beta_{11} & \beta_{13} \\ \beta_{13} & \beta_{33} \end{array} \right| \geq 0, \quad \left| \begin{array}{cc} \beta_{11} & \beta_{12} \\ \beta_{12} & \beta_{22} \end{array} \right| \geq 0, \\ \left| \begin{array}{ccc} \beta_{11} & \beta_{12} & \beta_{13} \\ \beta_{12} & \beta_{22} & \beta_{23} \\ \beta_{13} & \beta_{23} & \beta_{33} \end{array} \right| &\geq 0.\end{aligned}$$

Failure of one of these tests means that the coefficients do not represent physical reality. In this case an indicator is set to terminate the job, and a statement is put out describing the error.

Upon return from TEST, if the control integer IT  $\neq 0$ , the new parameters are put out on an auxiliary magnetic tape in the same format as the parameter input. This tape may be used to punch cards for input to future jobs, or the tape itself may serve as this input.

Unless the job is ended by TEST or unless a singular matrix has been found, the least-squares procedure will be repeated for the specified number of cycles, and then a final calculation and output of  $s_q F$  or  $(s_q F)^2$  will be made.

If a singular matrix has not been found, the program computes the correlation matrix by dividing each inverse matrix element AM(IJ) by SQRTF(DIAG(I)\*DIAG(J)) when the refinement is terminated. Only the upper triangular part of this symmetric matrix is reported, and the other elements appear as zero in the listing.

At the end of the job, if the control integer IXFE = 1, and if the matrix is not singular, a tape is written for use by the function and error program, OR FFE . (W. R. Busing, K. O. Martin, and H. A. Levy, "OR FFE, A Fortran Crystallographic Function and Error Program," ORNL-TM-306, 1962). This tape includes the final parameters, the variance-covariance matrix, and other quantities needed for the calculation of interatomic distances, angles, principal

thermal displacements, etc., and the standard errors of these quantities.

#### SYMMETRY CONSIDERATIONS

In the expressions for A and B, the terms  $\cos_{ij}$  and  $\sin_{ij}$  are the trigonometric contributions of the  $i$ th atom transformed to the  $j$ th equivalent position, and  $\exp_{ij}$  is the anisotropic temperature factor for this atom. OR FLS sets either  $\exp(-T_1\rho)$  or  $\exp_{ij}$  to unity, depending on the kind of temperature factor to be used.

The trigonometric contribution  $\cos_{ij}$  could be computed as

$$\cos_{ij} = \cos 2\pi(hx_{ij} + ky_{ij} + \ell z_{ij}).$$

Here  $h$ ,  $k$ , and  $\ell$  are the indices and  $x_{ij}$ ,  $y_{ij}$ , and  $z_{ij}$  are the coordinates of the  $i$ th atom in the asymmetric unit transformed to the  $j$ th equivalent position. OR FLS does not do this, however. Instead of transforming the coordinates, the indices  $h$ ,  $k$ , and  $\ell$  are transformed in a way which makes the result identical with the above:

$$\cos_{ij} = \cos 2\pi(h_j x_i + k_j y_i + \ell_j z_i + t_j).$$

Here  $x_i$ ,  $y_i$ , and  $z_i$  are the (untransformed) coordinates for the  $i$ th atom in the asymmetric unit;  $h_j$ ,  $k_j$ , and  $\ell_j$  are the transformed indices; and  $t_j$  is a translational term. As an example, we will illustrate the transformations used for the general positions of space group P3<sub>2</sub>2. Substitution of these quantities in the two expressions for  $\cos_{ij}$  will give identical results. The expression for  $\sin_{ij}$  is obtained in an analogous way.

j	x <sub>j</sub>	y <sub>j</sub>	z <sub>j</sub>	h <sub>j</sub>	k <sub>j</sub>	l <sub>j</sub>	t <sub>j</sub>
1	x	y	z	h	k	l	0
2	x-y	-y	-z	h	-h-k	-l	0
3	y-x	-x	1/3 + z	-h-k	h	l	l/3
4	-x	y-x	1/3 - z	-h-k	k	-l	l/3
5	-y	x-y	2/3 + z	k	-h-k	l	2l/3
6	y	x	2/3 - z	k	h	-l	2l/3

OR FLS permits any desired symmetry to be introduced by means of symmetry cards included as input data. There is one such card for each j value, and it consists of a statement of the coordinate transformations (as in the left half of the above table). The program automatically transforms the indices in ways which are equivalent to the coordinate transformations specified.

The anisotropic temperature factor,  $\exp_{ij}$ , is handled similarly. The fundamental expression is

$$\exp_{ij} = \exp\left\{ -[h^2\beta_{11}^{ij} + k^2\beta_{22}^{ij} + l^2\beta_{33}^{ij} + 2hk\beta_{12}^{ij} + 2hl\beta_{13}^{ij} + 2kl\beta_{23}^{ij}] \right\}$$

where  $\beta_{11}^{ij}$ , etc., are the six temperature factor coefficients for the i<sup>th</sup> atom of the asymmetric unit transformed to the j<sup>th</sup> equivalent position. Again the program makes the computation by transforming the index products rather than the coefficients themselves so that

$$\exp_{ij} = \exp\left\{ -[(h^2)_{j\frac{i_1}{i}} + (k^2)_{j\frac{i_2}{i}} + (\ell^2)_{j\frac{i_3}{i}} + (2hk)_{j\frac{i_1+i_2}{i}} + (2h\ell)_{j\frac{i_1+i_3}{i}} + (2k\ell)_{j\frac{i_2+i_3}{i}}] \right\}.$$

Here  $(h^2)_{j\frac{i_1}{i}}$ , etc., are the transformed index products which make the two expressions identical.

Rules for obtaining the transformed coefficients  $\beta_{ij}$ , etc., for any space group have been given by H. A. Levy (Acta Cryst. (1956) 9, 679). From these rules it may be deduced that for atoms in general positions  $(h^2)_{j\frac{i_1}{i}} = (h_j)^2$ , etc., so that the transformed index products are simply the products of the transformed indices. This is not necessarily true for atoms in special positions, however. OR FLS computes the products of transformed indices and assumes that  $(h^2)_{j\frac{i_1}{i}} = (h_j)^2$ , etc., and therefore the computed anisotropic temperature factor may not be valid for atoms in special positions.

#### Cells with translational symmetry (centering)

The specification of symmetry in the case of face-centered, end-centered, or body-centered cells can be simplified (and the computing time reduced) provided that the reflections which are extinguished by centering are not computed. Similar considerations apply to a rhombohedral cell described by hexagonal coordinates. In these cases, symmetry cards need be supplied only for positions not related by translation. The atom multipliers should then be increased by the appropriate factor.

Special positions

The ways of performing the computation when atoms are in special positions will now be considered. The important effects of atoms being in special positions are (a) that the number of these atoms is smaller than if they were in general positions, (b) that there are certain restrictions on the position parameters, and (c) that there may be some restrictions on the anisotropic temperature factor coefficients. No restrictions on isotropic temperature factors are introduced, however.

The ways of treating special positions with OR FLS depend on several factors: (1) whether all the atoms are in the same kind of special position, (2) whether the position parameters have a fixed value or whether there is a relationship among two or more coordinates, (3) whether anisotropic temperature factors are used or not, and (4) if they are used, whether there are (a) no restrictions on the coefficients, (b) certain coefficients fixed at zero, or (c) a relationship between two or more coefficients. H. A. Levy (loc. cit.) has given a rule for determining the restrictions on the anisotropic temperature factor coefficients of atoms in special positions.

Fixed parameters. When coordinates or temperature factor coefficients have fixed values, these values may be put into the list of trial parameters, and the parameter selection cards are prepared so that these parameters are not varied.

Symmetry cards for the general positions are used so that anisotropic temperature factors are correctly computed.

Symmetry cards for special positions. If all atoms are in the same kind of special position, and if anisotropic temperature factors are not used, then the correct result will be obtained by using symmetry cards for the special positions. For example, the space group  $P3_2\bar{2}$  mentioned above has special positions for  $y = x$ ,  $z = 1/3$  with the transformations:

j	$x_j$	$y_j$	$z_j$
1	x	x	1/3
2	0	-x	2/3
3	-x	0	0

This information can be introduced with three symmetry cards instead of using six for the general positions. All coordinates y and z in the parameter input are then irrelevant, and no attempt may be made to vary them.

Writing a special subroutine. It is possible to treat any symmetry situation which can arise by using symmetry cards for the general positions, allowing the program to compute the transformed indices and the index products which would be valid for these general positions, and then causing the program to modify these transformed indices appropriately by means of a specially prepared subroutine. Consider, for

example, the special positions mentioned above. The basic program alone would produce the trigonometric argument

$$h_j x_i + k_j y_i + \ell_j z_i + t_j.$$

If  $x_i$  is assumed to be the independent variable, then  $y_i = x_i$  and  $z_i = 1/3$ . Substituting these in the argument yields

$$h_j x_i + k_j x_i + \ell_j / 3 + t_j.$$

The program will produce this result if a subroutine is provided to replace  $h_j$  by  $h'_j = h_j + k_j$ ,  $k_j$  by  $k'_j = 0$ ,  $\ell_j$  by  $\ell'_j = 0$ , and  $t_j$  by  $t'_j = t_j + \ell_j / 3$ . The parameters  $y$  and  $z$  will again be irrelevant and must not be varied.

The restrictions on the anisotropic temperature factor coefficients may be handled in a similar way. For the atoms in the above example, Levy's rule shows that  $\beta_{zz} = \beta_{11}$ ,  $\beta_{z3} = -\beta_{13}$ . Taking  $\beta_{11}$  and  $\beta_{13}$  as independent, the transformations to be performed by the subroutine are:

$$\begin{aligned}(h^2)_j' &= (h^2)_j + (k^2)_j \\(k^2)_j' &= 0 \\(\ell^2)_j' &= (\ell^2)_j \\(2hk)_j' &= (2hk)_j \\(2h\ell)_j' &= (2h\ell)_j - (2k\ell)_j \\(2k\ell)_j' &= 0.\end{aligned}$$

In this case  $\beta_{zz}$  and  $\beta_{z3}$  are irrelevant and must not be varied.

One subroutine named PATCH may be prepared by the user to transform both the indices and the index products. Specifications for this subprogram are given below.

Although the parameters  $y$ ,  $\beta_{zz}$ , and  $\beta_{z3}$  in the above

example are irrelevant, it may be desirable to reset  $y = x$ ,  $\beta_{22} = \beta_{11}$ , and  $\beta_{23} = -\beta_{13}$  at the end of each cycle. In the case of the anisotropic temperature factor coefficients, this is necessary if the test for positive-definite form is to be valid. To provide for such resetting, the program calls two subroutines named RESETX and RESETB which may be prepared by the user according to specifications given below.

There is no reason why a combination of the fixed parameter and special subroutine methods may not be used. In the above example the z parameters could be fixed at 1/3 while the subroutine provides for the restriction,  $y = x$ . It may also be possible to choose a coordinate system which simplifies the restrictions on the parameters.

Correcting the number of atoms. The program as written always sums over all the equivalent positions specified by the symmetry cards. Thus the effective number of times an atom is included is equal to the number of symmetry cards for non-centrosymmetric structures and twice that number for centrosymmetric structures. If the symmetry cards describe the general positions, then atoms in special positions may be put in correctly by using the appropriate atom multiplier. When the symmetry cards are written for the special positions directly, an atom multiplier of unity will usually be correct.

### SPECIFICATIONS FOR SUBROUTINES

This section will give the specifications for the three subroutines which may be needed when atoms are in special positions. The purpose of these subprograms has been discussed in the previous section, and examples of such routines are included in the test problem which is provided. This problem is a hypothetical one based on alpha quartz with space group  $P\bar{3}_12$ , and the general and special positions used as examples earlier correspond to the positions of oxygen and silicon atoms, respectively.

#### PATCH(I,TJ,HJ,HHJ)

In the calculation of one structure factor, this routine will be called NA times for each of the NS symmetry positions. On each entry the argument I defines the atom which is being considered so that  $I = 1, 2, \dots, NA$  on successive entries for a given symmetry position.

The remaining arguments represent the transformed indices and index products as described in the glossary. On the first entry for each symmetry position, that is, for  $I = 1$ , these arguments will have been set by the program according to the information on one symmetry card. It is the task of this subroutine to modify these quantities appropriately. On successive entries for the same symmetry position these arguments will retain the values set previously by the subroutine. The main program does not reset them until it advances to a new symmetry position.

The array HHJ is irrelevant when isotropic temperature factors are used, so that no difficulty will be incurred by including a subroutine prepared for the anisotropic case in an isotropic refinement.

The statements required may be outlined as follows:

```
SUBROUTINE PATCH(I,TJ,HJ,HHJ)
DIMENSION HJ(3), HHJ(6)
```

Interrogate I with one or more IF statements to determine whether the values of the arguments are to be modified.

Set the values of the arguments appropriately.

```
RETURN
```

```
END
```

The subroutine should be compiled and substituted for the dummy program which is included with the card deck provided.

```
RESETX(XYZ)
```

This subroutine is called once near the end of each cycle of least squares. It is entered after the main output of the adjusted parameters but before the auxiliary output on cards or tape.

The array XYZ contains the atomic coordinates as described in the glossary. The statements to be included may be summarized as follows:

```
SUBROUTINE RESETX(XYZ)
```

```
DIMENSION XYZ(3,20)
```

Set the values of the constrained coordinates equal to the appropriate functions of the parameters which have been adjusted.

```
RETURN
```

```
END
```

The subroutine should be compiled and substituted for the dummy program which is included with the card deck provided.

```
RESETB(BETA)
```

This subroutine is called once near the end of each cycle except that it is not called when isotropic temperature factors are used. It is entered after the main output of the adjusted parameters but before the tests for positive-definite form and before the auxiliary output on cards or tape.

The array BETA contains the anisotropic temperature factor coefficients as described in the glossary. The statements to be included may be summarized as follows:

```
SUBROUTINE RESETB(BETA)
```

```
DIMENSION BETA(6,20)
```

Set the values of the constrained coefficients equal to the appropriate functions of those which have been adjusted.

RETURN

END

The subroutine should be compiled and substituted for the dummy program which is included with the card deck provided.

#### POSSIBLE CAUSES OF A SINGULAR MATRIX

A singular matrix may be the result of one of several kinds of errors in the input data. When one or more zero diagonal elements are found in the original matrix, the following sources of error should be considered:

1) Attempting to vary some undetermined parameter, for example, a z-coordinate, when only hk0 data are used.

2) Attempting to vary a parameter which should be fixed because an atom is in a special position.

A singular matrix with no zero diagonal elements may be the result of one of the following errors:

3) Attempting to vary more parameters than there are observations. An error in weighting could cause this difficulty.

4) Attempting to vary redundant parameters such as the over-all temperature factor and all the individual atom temperature factors, or the coordinates of all atoms when the origin is not fixed by the symmetry.

The singularity without zero diagonal elements is more difficult to diagnose. If other approaches fail, the redundant parameters can always be identified by trying refinements with various parameters held constant.

In either case, the output of the trial parameters and parameter selection integers should be checked, as the difficulty may simply be the result of a mistake on these input cards.

#### CAPACITY AND ARRAY DIMENSIONS

The user may wish to recompile the program with modified DIMENSION statements in order to allocate storage for a particular problem. The following table illustrates the way in which the storage used by the arrays depends on the different variables. The figures included correspond to the dimensions in the program as distributed.

Maximum Values		Storage Used	
NV	100	$5*NV + NV*(NV + 3)/2$	5650
NP	230	$3*NP$	690
NO	2500	$6*NO$	15000
NA	20	$45*NA$	900
NQ	9	$2*NQ$	18
NF	10	$32*NF$	320
NS	24	$9*NS$	<u>216</u>
		Total	22794

The number of locations occupied by the complete program with temporary storage not listed above is about 6500. This

leaves approximately 3400 locations for use by the monitor system, for subroutines added by the user, or for expansion of the capacity of the program.

For large problems a simple modification may be made which will remove all restrictions from NO and allow NV to increase to about 200. Since the observations are used one at a time, the values of X, YO, and SIGYO may be written on magnetic tape at input time, one observation to a record, and read back for use during the loop through the observations.

Another approach to large problems would be to vary different blocks of parameters successively. For this purpose the user may wish to modify the program to read parameter selection cards at the beginning of each cycle.

#### DATA INPUT

The limitations marked with an asterisk (\*) depend only on the dimensions with which the program is compiled.

1. Title card. FORMAT(12A6)  
Columns  
1-72      Title consisting of any desired Hollerith information. This will be put out as a heading on each section of output.
2. Control cards.  
First card FORMAT(6I3)  
Columns  
1-3      NC, the number of cycles to be run on this job. Calculated values of YC, the scaled structure factor or its square, will be listed NC + 1 times. If NC = 0, one list of YC will be put out, but no refinement will be made.
- 4-6      NV, the number of parameters to be varied.  
If NC = 0, then NV is irrelevant.  
 $1 \leq NV \leq 100.*$

## Columns

7-9

IW, the weight indicator. IW = 0 indicates that individual standard errors will be supplied by the user for each observation. IW = 1 indicates that the program is to weight each observation at unity.

10-12

IP, the parameter input indicator. If IP = 0, the trial parameters P are to be read as input data. If IP > 0, then the parameters are to be taken from the magnetic tape output of cycle IP of a previous job.

13-15

IT, the parameter output indicator. If IT = 0, parameters are not to be written on tape for use as input to later least-squares cycles. If IT = 1, they are to be written on a private tape. If IT = 2, they are written on the monitor auxiliary tape in such a way as to yield punched cards. The private tape is initially rewound and is terminated by an end-of-file while the auxiliary tape is not.

16-18

IXFE, the function and error output indicator. If IXFE = 1, information including the parameters and the variance-covariance matrix will be written on a private tape for use by OR FFE. If IXFE = 0, no such output will be made.

## Second card

## Columns

1-3

## FORMAT(7I3)

IFSQ, the  $F^2$  indicator. If IFSQ = 1, the program calculates  $s_q F$ . If IFSQ = 2, the program calculates  $(s_q F)^2$ .

4-6

ITF, the temperature factor indicator. ITF = 1 for isotropic temperature factors. ITF = 2 for anisotropic temperature factors. If ITF = 3, the program converts isotropic temperature factor coefficients to anisotropic form before refining.

7-9

NF, the number of different x-ray form factor tables to be used. For neutron diffraction NF = 0.  $0 \leq NF \leq 10.*$

10-12

NA, the number of atoms in the asymmetric unit.  $1 \leq NA \leq 20.*$

## Columns

13-15

ICENT, the symmetry indicator. ICENT = 1 indicates a centrosymmetric structure with the origin at a symmetry center. ICENT = 2 indicates a non-centrosymmetric structure.

16-18

NS, the number of symmetry cards. For non-centrosymmetric structures NS is equal to the number of equivalent positions. For centrosymmetric structures NS is equal to one-half the number of equivalent positions.  $1 \leq NS \leq 24.*$

19-21

NQ, the number of scale factors in the parameter list.  $1 \leq NQ \leq 9.*$

3. Scattering factor tables. **FORMAT(8F9.3)**

Four cards are to be provided for each of NF tables. For neutron diffraction problems NF = 0, and these cards are omitted. Entries beyond the range needed for linear interpolation may be left blank.

## First card

## Columns

1-9

Scattering factor for  $\sin\theta/\lambda = 0.00$

10-18

Scattering factor for  $\sin\theta/\lambda = 0.05$

.

.

.

64-72

Scattering factor for  $\sin\theta/\lambda = 0.35$

## Second card

## Columns

1-9

Scattering factor for  $\sin\theta/\lambda = 0.40$

.

.

.

## Third card

## Columns

1-9

Scattering factor for  $\sin\theta/\lambda = 0.80$

.

.

.

## Fourth card

## Columns

1-9

Scattering factor for  $\sin\theta/\lambda = 1.20$

.

.

.

64-72

Scattering factor for  $\sin\theta/\lambda = 1.55$

4. Symmetry cards. FORMAT(F11.6,2I2,F11.6,2I2,F11.6,2I2)  
 Each of these NS cards describes one symmetry transformation  $j$  of the atomic coordinates. For non-centro-symmetric structures, NS is the number of equivalent positions. For centrosymmetric structures (with the origin at a center), NS is half the number of equivalent positions, and only one position of each centrosymmetrically related pair is used. The basic position  $x, y, z$  must be included in these cards. See the sample problem for an example of this input.

## Columns

1-11	Translational part of $x_j$ or blank.
12-13	1, 2, 3, -1, -2, -3, or blank for $x, y, z, -x, -y, -z$ , or blank, respectively, as used in the expression for the transformed $x_j$ .
14-15	1, 2, 3, -1, -2, -3, or blank for $x, y, z, -x, -y, -z$ , or blank, respectively, as used in the expression for the transformed $x_j$ . (Columns 12 and 13 are exactly equivalent to 14 and 15. Also, note that an expression such as $x_j = 2x$ must be treated as $x_j = x + x$ .)
16-26	Translational part of $y_j$ or blank.
27-30	Integers representing plus or minus $x, y, z$ in the expression for the transformed $y_j$ as described above.
31-41	Translational part of $z_j$ or blank.
42-45	Integers representing plus or minus $x, y, z$ in the expression for the transformed $z_j$ .

5. Reciprocal cell data card. FORMAT(6F9.6)

## Columns

1-9	a* in reciprocal Angstroms
10-18	b* in reciprocal Angstroms
19-27	c* in reciprocal Angstroms
28-36	$\cos\alpha^*$
37-45	$\cos\beta^*$
46-54	$\cos\gamma^*$

## 6. Trial parameter cards.

These cards are included only if IP = 0. Otherwise the trial parameters (in exactly the same format) will be read from the magnetic tape output of cycle IP of a previous job.

## A. Scale factor cards. FORMAT(8F9.6)

## Columns

1-9	First scale factor, $s_1$ .
10-18	Second scale factor, $s_2$ .
.	.
.	.
.	.
64-72	Eighth scale factor, $s_8$ .

The scale factors are continued on additional cards if there are more than eight of them.

## B. Over-all temperature factor card. FORMAT(F9.6)

## Columns

1-9	$T_o$ , the coefficient for the over-all temperature factor $\exp(-T_o \sin^2 \theta / \lambda^2)$ .
-----	--

## C. Atom parameter cards.

Two cards are needed for each atom i in the asymmetric unit, where i = 1, 2, ..., NA.

## First card FORMAT(A6,3X,5F9.6)

## Columns

1-6	Any 6 Hollerith characters identifying atom i. These will be printed with the parameter output.
7-9	Blank
10-18	X-ray scattering factor identifier or neutron scattering factor. For x-ray problems (NF ≠ 0) this is an integer from one to NF which identifies the scattering factor table to be used for atom i. The scattering factor tables are numbered in the order in which they were read. Include a decimal point after this number.

For neutron problems (NF = 0) this is the neutron scattering factor itself.

Columns 19-27 A multiplier,  $a_i$ , applied to the scattering factor of atom i. This number will usually be 1.0 unless symmetry considerations dictate otherwise.

28-36 The coordinate  $x_i$  for atom i.

37-45 The coordinate  $y_i$  for atom i.

46-54 The coordinate  $z_i$  for atom i.

For isotropic temperature factors (or for isotropic temperature factors converted to anisotropic form before refining):

## Columns

1-9       $T_i$ , the coefficient for the isotropic temperature factor for atom i,  
 $\exp(-T_i \sin^2 \theta / \lambda^2)$ .

For anisotropic temperature factors:

## Columns

1-9  $\beta_{11i}$ , a coefficient in the expression for the anisotropic temperature factor for atom  $i$ ,  $\exp[-(\beta_{11i}h^2 + \beta_{22i}k^2 + \beta_{33i}\ell^2 + 2\beta_{12i}hk + 2\beta_{13i}h\ell + 2\beta_{23i}k\ell)]$ .

10-18  $\beta_{22j}$

19-27  $\beta_{33j}$

28-36  $\beta_{1,2,i}$

37-45  $\beta_{13j}$

46-54  $\beta_{23}$

7. Reflection data cards. FORMAT(I1,F8.0,5F9.0)  
 One card is needed for each reflection observed or for  
 each structure factor to be computed.  
 $1 \leq NO \leq 2499.*$

## Columns

Blank

2-9 The index h. No decimal point is needed.

10-18 The index k. No decimal point is needed.

Columns	
19-27	The index $\ell$ . No decimal point is needed.
28-36	The observed value of $ F $ or $F^2$ , whichever is being refined. For structure factor calculations this field may be left blank.
37-45	The standard error of this observation. If IW = 1 on the control card, this field is irrelevant.
46-54	$q$ , where $1 \leq q \leq NQ$ and $s_q$ is the scale factor to be used in computing this reflection. No decimal point is needed.

8. Observation termination card.      FORMAT(11)

Column	
1	1 as a sentinel for the end of the observation deck.

9. Parameter selection cards.      FORMAT(7211)

These cards specify the NV parameters to be varied. Consider the trial parameters to be stored in the array P in the following order: the NQ scale factors, the over-all temperature factor coefficient, the six or eleven parameters for the first atom, those for the second atom, etc. The parameters for each atom are the scattering factor, the multiplier, the three coordinates, and the one or six temperature factor coefficients. Each column of the parameter selection card contains an integer KI(I) so that if  $KI(I) = 0$ , then  $P(I)$  will be held constant. If  $KI(I) = 1$ , then  $P(I)$  will be adjusted.

Six temperature factor coefficients per atom should be assumed if anisotropic temperature factors are specified or if isotropic temperature factors are to be converted to anisotropic form before refining. For isotropic refinements there is only one temperature factor per atom.

Note that for both x-ray and neutron problems the scattering factor is considered to be a parameter. The neutron scattering factor may be adjusted by least squares, but varying an x-ray scattering factor must not be attempted.

First card

Column

1	KI(1)
2	KI(2)
.	.
.	.
.	.
72	KI(72)

Second card  
 Column  
 1                    KI(73)  
 .                    .  
 .                    .  
 .                    .  
 .                    .  
 .                    KI(NP)

#### TAPES REQUIRED

Listed here are the monitor tape control cards required for operation at the Oak Ridge Central Data Processing Facility. At other installations the necessary tapes should be specified appropriately.

##### \*TAPE(3, POOL, SAVE)

This is required only if IXFE = 1, indicating that data for the Function and Error Program, OR FFE, are to be saved on tape after the final cycle of refinement. This tape is initially rewound and an end-of-file is written upon completion of the job.

##### \*TAPE(4, Reel number, SAVE)

This is required only if IP > 0, indicating that the initial values of the trial parameters are to be taken from this tape, which was written on a previous job.

##### \*TAPE(5, POOL, SAVE)

This is required only if IT = 1, indicating that the adjusted parameters are to be written on this tape after each cycle. This tape is initially rewound and an end-of-file is written upon completion of the job.

##### \*TAPE(6, AUXOUT)

This is required only if IT = 2, indicating that the adjusted parameters are to be written on this tape

**\*TAPE(6, AUXOUT) Continued**

after each cycle. Cards suitable for input to another job will then be punched off-line. This tape is not rewound and no end-of-file is written on it by the program.

**\*TAPE(9, OUTPUT)**

This is the monitor output tape to be listed.

**\*TAPE(10, INPUT)**

This is the monitor input tape prepared from cards.

**CARD DECKS PROVIDED**

<u>Subprogram</u>	<u>Type</u>	<u>Symbolic card numbers</u>	<u>Column binary card numbers</u>
Calling program	Fortran	1 - 474	1472 - 1560*, †
PRELIM	Fortran	475 - 629	1561 - 1590*
CALC	Fortran	630 - 929	1591 - 1636*
TEST	Fortran	930 - 1018	1637 - 1649*
PTOSB	Fortran	1019 - 1058	1650 - 1658
SBTOP	Fortran	1059 - 1098	1659 - 1667
SMI	FAP	1099 - 1351	1668 - 1681
PATCH (dummy)	Fortran	1352 - 1358	1682 - 1683
RESETX (dummy)	Fortran	1359 - 1365	1684 - 1685
RESETB (dummy)	Fortran	1366 - 1372	1686 - 1687

\*The column binary cards provided were compiled and assembled on an IBM 7090. The calling program, PRELIM, CALC, and TEST should be recompiled if they are to be used on an IBM 704, but the remaining subprograms should work satisfactorily on either machine.

†Card No. 1472 is a control card for the Oak Ridge Monitor System. It may not be appropriate at other installations.

Subprogram	Type	Symbolic card numbers	Column binary card numbers
Library routines SQRT, SIN, COS, EXP, and EXIT (which terminates the job) should be inserted here if they are not supplied by the monitor system.			
PATCH (example)	Fortran	1373 - 1389	1688 - 1692
RESETX (example)	Fortran	1390 - 1398	1693 - 1695
RESETB (example)	Fortran	1399 - 1408	1696 - 1698
Transfer card		1409	
Permanent data cards		1410 - 1412†	
Data for example		1413 - 1471	

†These cards must be present on all problems.

#### GLOSSARY OF SYMBOLS

Arrays are represented by symbols followed by their minimum allowable dimensions. All other symbols refer to single storage variables. Those marked with an asterisk (\*) are read as input data.

A	Real component of the structure factor.
*AI(NA)	Atom multipliers, $a_i$ .
AM((NV*(NV+3))/2)	Matrix of the normal equations. This area is also used for the inverse matrix. Only $(NV*(NV+1))/2$ words are used for the matrix, but NV more are used by the inverter. Only the upper right triangle of the matrix is stored, and this is stored forward in the memory - i.e., backward in the Fortran indexing system. If $a_{ij}$ represents a matrix element, then $a_{11}$ is at AM((NV*(NV+1))/2), $a_{12}$ is at AM((NV*(NV+1))/2-1), etc., $a_{22}$ is at AM((NV*(NV+1))/2-NV), and $a_{NV,NV}$ is at AM(1). For example, if NV = 4, the storage is as illustrated:

$a_{11} = AM(10)$	$a_{12} = AM(9)$	$a_{13} = AM(8)$	$a_{14} = AM(7)$
	$a_{22} = AM(6)$	$a_{23} = AM(5)$	$a_{24} = AM(4)$
		$a_{33} = AM(3)$	$a_{34} = AM(2)$
			$a_{44} = AM(1)$

*ATOM(NA)	Alphanumeric name of each atom read in with the parameters of that atom and used in the output as a heading for those parameters.
B	Imaginary component of the structure factor.
*BETA(6,NA)	Anisotropic temperature factor coefficients $\beta_{11}$ , $\beta_{22}$ , $\beta_{33}$ , $\beta_{12}$ , $\beta_{13}$ , $\beta_{23}$ (in that order) for the NA atoms. If isotropic temperature factors are used, then BETA(1,I) is the coefficient for atom I.
CA	Coefficient of $\partial A / \partial p$ in the expression for $\partial(s_q F) / \partial p$ or $\partial(s_q^2 F^2) / \partial p$ .
CB	Coefficient of $\partial B / \partial p$ in the expression for $\partial(s_q F) / \partial p$ or $\partial(s_q^2 F^2) / \partial p$ .
COSIJ	Trigonometric contribution of atom I in symmetry position J. Also used for COSIJ*EXP(IJ).
DADAI(NA)	$\partial A / \partial a_i$ - This array is also used for $\sum f_i \cos_{ij} \exp_{ij}$ .
DADB(6,NA)	$\partial A / \partial \beta_{11j}$ , etc. - This array is also used for $\sum h_j^2 \cos_{ij} \exp_{ij}$ , etc.
DADFI(NA)	$\partial A / \partial f_i$ - This array is also used for $\sum \cos_{ij} \exp_{ij}$ .

DADX(3,NA)	$\partial A / \partial x_i$ , $\partial A / \partial y_i$ , and $\partial A / \partial z_i$ - This array is also used for $\sum_j h_j \sin_{ij} \exp_{ij}$ , etc.
DBDAI(NA)	$\partial B / \partial a_i$ - This array is also used for $\sum_j f_i \sin_{ij} \exp_{ij}$ .
DBDB(6,NA)	$\partial B / \partial \beta_{11i}$ , etc. - This array is also used for $\sum_j h_j^2 \sin_{ij} \exp_{ij}$ , etc.
DBDFI(NA)	$\partial B / \partial f_i$ - This array is also used for $\sum_j \sin_{ij} \exp_{ij}$ .
DBDX(3,NA)	$\partial B / \partial x_i$ , $\partial B / \partial y_i$ , and $\partial B / \partial z_i$ - This array is also used for $\sum_j h_j \cos_{ij} \exp_{ij}$ , etc.
DC(NP)	Calculated derivatives of YC with respect to all parameters p.
DFDAI(NA)	$\partial(s_q F) / \partial a_i$ or $\partial(s_q^2 F^2) / \partial a_i$ - Later copied to array DC.
DFDB(6,NA)	$\partial(s_q F) / \partial \beta_{11i}$ , etc., or $\partial(s_q^2 F^2) / \partial \beta_{11i}$ , etc. Later copied to DC. When isotropic temperature factors are specified, DFDB(1,I) is used for $\partial(s_q F) / \partial T_i$ or $\partial(s_q^2 F^2) / \partial T_i$ .
DFDFI(NA)	$\partial(s_q F) / \partial f_i$ or $\partial(s_q^2 F^2) / \partial f_i$ . Later copied to array DC.
DFDS(NQ)	$\partial(s_q F) / \partial s_q$ or $\partial(s_q^2 F^2) / \partial s_q$ . Later copied to array DC.
DFDTO	$\partial(s_q F) / \partial T_o$ or $\partial(s_q^2 F^2) / \partial T_o$ .
DFDX(3,NA)	$\partial(s_q F) / \partial x_i$ , etc., or $\partial(s_q^2 F^2) / \partial x_i$ , etc. Later copied to DC.
DIAG(NV)	Diagonal elements of the inverse matrix. These are used for calculating the standard errors of the parameters which were varied.
DV(NV)	Derivatives of those parameters which are to be varied, multiplied by the square root of the weight.

DY	$YO(I) - YC$ .
EXPIJ	Anisotropic temperature factor for atom I in symmetry position J.
F	$s_q F$ or $s_q^2 F^2$ . F is then copied to YC.
FI	Atomic scattering factor, $f_i$ . Also used for $f_i \exp(-T_i \rho)$ and for $-f_i \exp(-T_i \rho)$ .
FRACPT	Fractional part of PT.
FTA	$a_i f_i$ for anisotropic temperature factors, or $a_i f_i \exp(-T_i \rho)$ for isotropic temperature factors.
FTACOS	$a_i f_i \exp(-T_i \rho) \sum_j \cos_{ij}$ .
FTASIN	$a_i f_i \exp(-T_i \rho) \sum_j \sin_{ij}$ .
*FX(32,NF)	Scattering factor tables.
*H(4)	Untransformed indices h, k, and l, and the scale factor specification, q. H is the same as column I or array X.
HHB	Exponential argument.
HHJ(6)	Transformed index products $(h^2)_j$ , $(k^2)_j$ , $(l^2)_j$ , $(2hk)_j$ , $(2hl)_j$ , and $(2kl)_j$ in that order.
HJ(3)	Transformed indices $h_j$ , $k_j$ , and $l_j$ .
HOLD	Temporary location used in reversing the order of elements of matrix AM.
HX	Trigonometric argument, $h_j x_i + k_j y_i + l_j z_i + t_j$ .
IC	Identifying number of a particular cycle in the job.
*ICENT	Symmetry indicator. ICENT = 1 for centrosymmetric structures. ICENT = 2 for non-centrosymmetric structures.
*IFSQ	$F^2$ indicator. If IFSQ = 1 the refinement is based on the scaled structure factors. If IFSQ = 2 the squares of these quantities are used.

IHKL(4)	The array X(4,NO) converted to fixed point numbers for output purposes.
II	Index used so that AM(II) is diagonal element $a_{ii}$ .
IID	Increment subtracted from II to step down diagonal of matrix AM(II).
IJ	Index used so that AM(IJ) is $a_{ij}$ .
IJD	Increment subtracted from IJ to step down a column of matrix AM(IJ).
*IP	Parameter input indicator. If IP = 0 the trial parameters p are to be read as input data. If IP > 0, the parameters are to be taken from the magnetic tape output of cycle IP of a previous job.
IPT	Integral part of PT.
IQ	Independent variable, q, specifying the scale factor, $s_q$ , associated with a given reflection.
*ISENT	Sentinel set at 1 to end the observation deck.
ISING	Singularity indicator set at 1 if a zero diagonal element is found in the original matrix or if a diagonal element becomes zero or negative during inversion by SMI. Otherwise ISING = 0.
*IS(2,3,NS)	Integers representing the non-translational part of the symmetry information. For example, if the Jth symmetry transformation is $y-x$ , $-x$ , $1/3 + z$ , this information would be stored as follows:
	<pre> TS(1,J)    = 0.0 IS(1,1,J)  = 2 (for y) IS(2,1,J)  = -1 (for -x) TS(2,J)    = 0.0 IS(1,2,J)  = -1 (for -x) IS(2,2,J)  = 0 TS(3,J)    = 0.333333 IS(1,3,J)  = 3 (for z) IS(2,3,J)  = 0 </pre>
ISTOP	Stop indicator set at 1 by subroutine TEST to indicate that no further cycles are to be run on this job. Otherwise ISTOP = 0.

*IT	Parameter output indicator. If IT = 0, parameters are not to be written on tape for use as input to later least-squares cycles. If IT = 1, they are to be written on a private tape. If IT = 2, they are written on the monitor auxiliary tape in such a way as to yield punched cards. The private tape is initially rewound and is terminated by an end-of-file while the auxiliary tape is not.
*ITF	Temperature factor indicator. ITF = 1 for isotropic temperature factors. ITF = 2 for anisotropic temperature factors. If ITF = 3, the program converts isotropic temperature factor coefficients to anisotropic form before refining.
*IW	Unit weight indicator. If IW = 1, all observations are assigned unit weights. If IW = 0, then the weights are taken as $1.0/\text{SIGY0}(I)^{**2}$ .
*IXFE	Function and error output indicator. If IXFE = 1, information including the parameters and the variance-covariance matrix will be written on a private tape for use by OR FFE. If IXFE = 0, no such output will be made.
JK	Index used so that AM(JK) is $a_{jk}$ .
*KI(NP)	Parameter selection integers. KI(I) = 1 if P(I) is to be varied. Otherwise KI(I) = 0.
*LABEL(2,14)	Alphanumeric labels read in at the start of the problem and used to label each parameter at the time of the output of the old and new parameters.
*NA	Number of atoms in the asymmetric unit.
*NC	Number of cycles of refinement to be performed in the job. The program puts out YC, the calculated values of the scaled structure factor or its square, NC + 1 times. If NC = 0, YC is calculated and put out, but no refinement occurs.
NCY	NC + 1, the number of cycles plus one. This is the number of times the list of YC will be put out.
*NF	Number of different x-ray form factor tables to be used. For neutron diffraction NF = 0.

NM	$(NV*(NV + 1))/2$ , the number of elements in the matrix AM.
NO	Number of observations.
NP	Total number of parameters including those to be varied as well as those to be held constant.
NPCD	Smallest multiple of 8 greater than or equal to NQ. Used for punching scale factors 8 to a card.
*NQ	Number of scale factors in the parameter list.
*NS	Number of symmetry cards. For non-centro-symmetric structures, NS is equal to the number of equivalent positions. For centro-symmetric structures, NS is half the number of equivalent positions.
NT	Number of private or auxiliary tape used for output of parameters to be saved.
*NV	Number of parameters to be varied. If NC = 0, then NV is irrelevant.
NX	Number of independent variables associated with each observation. NX is fixed at 4 in this program.
PDI	PD(I).
PD(NV)	Calculated parameter changes for those parameters which were varied.
PIFI	$-2\pi a_i f_i \exp(-T_i \rho)$ or $2\pi a_i f_i \exp(-T_i \rho)$ .
P(NP)	List of NP parameters, some of which will be varied. These are copied from various arrays by the subroutine SBTOP, adjusted, and then restored to the arrays by subroutine PTOSB.
POLD	Parameter before correction is added.
PRCP(6)	Products of the reciprocal cell parameters, $a^*{}^2/4$ , $b^*{}^2/4$ , $c^*{}^2/4$ , $a^*b^*\cos\gamma*/4$ , $a^*c^*\cos\beta*/4$ , $b^*c^*\cos\alpha*/4$ , in that order.
PT	$1.0 + (\sin\theta/\lambda)/.05$ . The location of FI in the scattering factor table, FX.
R	R factor in which the summations are made over all non-zero observations.

*RCP(6)	Reciprocal cell parameters, $a^*$ , $b^*$ , $c^*$ , $\cos\alpha^*$ , $\cos\beta^*$ , $\cos\gamma^*$ , in that order.
RHO	$\rho = (\sin\theta/\lambda)^2$ for each reflection.
RNUM	Numerator of R.
ROW(NV)	A row of the correlation matrix ready for output.
RZ	R factor in which the summations are made over all observations, including zero observations.
RZDEN	Denominator of both R and RZ.
RZNUM	Numerator of RZ.
*SC(NQ)	NQ scale factors.
*SF(NA)	For neutron problems, SF(I) is the scattering factor $f_i$ for atom I. For x-ray problems, it is an integer (in floating point form) which defines the scattering factor table to be used.
SIG	$(\text{SQRTW} * (Y_O(I) - Y_C))^{**2}$ summed over all observations.
SIGP	Standard error of a parameter.
*SIGYO(NO)	Standard errors of the NO observed structure factors or their squares.
SINIJ	Trigonometric contribution of atom I in position J. Also used for SINIJ*EXPIJ.
SINTHL	$\sin\theta/\lambda = \rho^{1/2}$ .
SQRTAB	$(A^2 + B^2)^{1/2}$ .
SQRTW	Square root of the weight for each observation.
SQSIG(2)	SQSIG(1) is the error of fit, SQRTF(SIG/FLOATF(NO-NV)). SQSIG(2) is SQSIG(1) saved from the previous cycle of this job. SQSIG(2) will be set to zero for the first cycle of each job.
SQTO	$s_q \exp(-T_O \rho)$ or $s_q^z \exp(-2T_O \rho)$ .
TFI	Isotropic temperature factor, $\exp(-T_i \rho)$ .
*TITLE(12)	Alphanumeric title read at start of problem and transcribed to the output.

TJ	Translational term, $t_j$ , for the trigonometric argument, HX.
*TO	Over-all temperature factor coefficient, $T_o$ .
*TS(3,NS)	Translational part of symmetry information. (See IS for an example.)
VARI	$SQSIG(1)**2$ , the constant used to convert the inverse matrix to the variance-covariance matrix.
V(NV)	Vector of the normal equations.
WDY	$(YO(I)-YC)/SIGYO(I)$ .
WR	Weighted R factor in which the summations are made over all non-zero observations.
WRNUM	Numerator of WR.
WRZ	Weighted R factor in which the summations are made over all observations, including zero observations.
WRZDEN	Denominator of both WR and WRZ.
WRZNUM	Numerator of WRZ.
*X(4,NO)	Four independent variables for each of NO observations. These are the indices h, k, and l and q, the number specifying the scale factor. The latter will be moved to IQ.
*XYZ(3,NA)	Atomic coordinates x, y, and z for the NA atoms.
YC	Calculated value of the scaled structure factor or its square stored by subroutine CALC.
*YO(NO)	NO observed structure factors or their squares.

## SYMBOLIC PROGRAM LISTING

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*TYPE(FORTRAN)                                FLS  1
C      OR FLS, FORTRAN CRYSTALLOGRAPHIC LEAST SQUARES      FLS  2
C      CALLING PROGRAM, A MODIFICATION OF OR GLS          FLS  3
COMMON NC,NV,NX,IW,IP,IT,NP,ISENT,NO,NM,NCY,IC,SIG,YC      FLS  4
COMMON SCRFw,CY,W0Y,JK,ISINC,FI,IID,PDI,II,JID,POLD      FLS  5
COMMON SIGP,ISTOP,AT,NPCD,EXFE,HOLD,VARI                 FLS  6
COMMON TITLE,P,X,Y,O,SIGYO,KI,SQSIG,AM,V,DC,CV,DIAG,PD,ROW      FLS  7
COMMON RNUM,RZNUM,RZDEN,WRNUM,WRZNUM,WRZDEN,R,RZ,WR,WRZ      FLS  8
COMMON LABEL,ATOM,IHKL                               FLS  9
COMMON IFSU,ITF,NF,NA,ICENT,NS,NQ,TU,TJ,HX,RHB,EXP1J,COSIJ,SINIJ      FLS 10
COMMON FI,A,B,RHO,SINH,L,PT,IFT,FRACPT,FTA,FTACOS,FTASIN,TFI,PIFI      FLS 11
COMMON IC,SQTO,SQRTAR,F,DFCTO                         FLS 12
COMMON SC,SF,AL,XYZ,PETA,DADCF,DCBDF,DAACAI,DAHAI,DAFX,DBDX,DADB      FLS 13
COMMON DCDA,DCDFS,DCFCF,DCFCAI,DCFCX,DCFB,TS,IS,HJ,HJJ,RCP,FX,PRCP      FLS 14
COMMON CA,CH                               FLS 15
C      DIMENSIONS FOR NV(MAX)#1DC,NP(MAX)#23D,NO(MAX)#25CE,NX(MAX)#4,      FLS 16
      NFMAX#1DC,NA(MAX)#2D,NS(MAX)#24,NQ(MAX)#9      FLS 17
DIMENSION TITLE(12),P(23D),X(4,25D),Y(25D),SIGYO(25D),KI(23D)      FLS 18
DIMENSION S0SIG(2),AM(515D),V1CC(1),DC(23D),DV(18D)      FLS 19
DIMENSION DIAG(1CD),PD(1CC),ROW(1CD),ATCM(2D),LABEL(2,14),IHKL(4)      FLS 20
DIMENSION D(12D),A(12D),XY(3,2D),BETA(6,2D),DADF(12D)      FLS 21
DIMENSION SC( 9),SF(12D),A(12D),XY(3,2D),BETA(6,2D),DADF(12D)      FLS 22
DIMENSION D(12D),DADAI(2D),DBDAI(2D),DADX(3,2D),DBDX(3,2D)      FLS 23
DIMENSION DADB(6,2D),DBCB(6,2D),DFDS( 9),DFDF(12D),CFDAI(2D)      FLS 24
DIMENSION DFDX(3,2D),CFCH(6,2D),TS(3,24),IS(2,3,24),HJ(3),H(4)      FLS 25
DIMENSION HJJ(6),RCP(6),FX(32,1C),PRCP(6)      FLS 26
                                         FLS 27
C      FORMAT STATEMENTS                                FLS 28
00031 FORMAT(18F9.6,12X)                           FLS 29
00032 FORMAT(F9.6,75X)                           FLS 30
00033 FORMAT(1A6,3X,5F9.6,3CX)                  FLS 31
00034 FORMAT(16F9.6,3CX)                           FLS 32
00035 FORMAT(16H0)INPUT DATA FOR OR-FORTRAN FUNCTION AND ERROR PROGRAM NOFLS 33
      IT TO BE SAVED)                                FLS 34
00037 FORMAT(15H0)INPUT DATA FOR OR-FORTRAN FUNCTION AND ERROR PROGRAM/ FLS 35
      13DH TO BE WRITTEN ON PRIVATE TAPE)            FLS 36
00041 FORMAT(1HGX,29HNUMERATOR      DENOMINATOR      R)      FLS 37
00042 FORMAT(125H0R FACTOR INCLUDING ZEROS,17X,F9.3,4X,F9.3,4X,F5.3)      FLS 38
00043 FORMAT(124H0R FACTOR OMITTING ZEROS,18X,F9.3,4X,F9.3,4X,F5.3)      FLS 39
00044 FORMAT(134H0WEIGHTED R FACTOR INCLUDING ZEROS,      FLS 40
      18X,F9.3,4X,F9.3,4X,F5.3)                  FLS 41
00046 FORMAT(133H0WEIGHTED R FACTOR OMITTING ZEROS,      FLS 42
      19X,F9.3,4X,F9.3,4X,F5.3)                  FLS 43
00051 FORMAT(12A6)                                FLS 44
00052 FORMAT(1H112A6)                            FLS 45
00053 FORMAT(124I3)                                FLS 46
00054 FORMAT(132H0NUMBER OF CYCLES IN THIS JOB IS12/37H0NUMBER OF PARAMETFLS 47
      FRS TO BE VARIED IS14)                          FLS 48
00061 FORMAT(3H0WEIGHTS TO BE SUPPLIED BY USER)        FLS 49
00062 FORMAT(34H0UNIT WEIGHTS TO BE SET BY PROGRAM)    FLS 50
00063 FORMAT(36H0PARAMETERS TO BE REAC AS INPUT DATA)   FLS 51
00064 FORMAT(34H0PARAMETERS TO BE TAKEN FRM CYCLEI2,16H OF PREVIOUS JOBFLS 52
      1)                                         FLS 53
00067 FORMAT(29H0NUMBER OF PARAMETERS READ IS14)        FLS 54
00068 FORMAT(1I,F8.0,7F9.0)                           FLS 55
00069 FORMAT(31H0NUMBER OF OBSERVATIONS READ IS15)      FLS 56
00070 FORMAT(172I1)                                FLS 57
00071 FORMAT(10F12.8)                                FLS 58
00072 FORMAT(46H0CALCULATED Y BASED CN PARAMETERS BEFORE CYCLEI2)      FLS 59
00073 FORMAT(97H0      H   K   L      Y(OBS)      Y(CALC)      A      B)      FLS 60
                                         FLS 60

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00223	WRITE OUTPUT TAPE 9,00035	FLS 121
	GO TO 00301	FLS 122
00225	WRITE OUTPUT TAPE 9,00037	FLS 123
	REWIND 3	FLS 124
C	ENTER PRELIM TO READ CRYSTALLOGRAPHIC INPUT	FLS 125
00301	CALL PRELIM	FLS 126
00601	WRITE OUTPUT TAPE 9,00067,NP	FLS 127
C	READ OBSERVATIONS TO SENTINEL	FLS 128
J#0		FLS 129
00801	J#J+1	FLS 130
	READ INPUT TAPE 10,00068,ISENT,(X(I,J),I#1,3),Y0(J),SIGYC(J),	FLS 131
I	X(4,J)	FLS 132
	IF(ISENT)00801,00801,01101	FLS 133
01101	NC#J-1	FLS 134
	WRITE OUTPUT TAPE 9,00069,NC	FLS 135
C	READ KEY INTEGERS IF REFINEMENT IS TO BE MADE	FLS 136
1F(NC)01601,01601,01301		FLS 137
01301	READ INPUT TAPE 10,00070,(KI(I),I#1,NP)	FLS 138
C	INITIALIZE PROBLEM	FLS 139
01601	NM#(NV*(NV+1))/2	FLS 140
	SQSIG(1)#0.0	FLS 141
C	PUT OUT TRIAL PARAMETERS AND KEY INTEGERS	FLS 142
	WRITE OUTPUT TAPE 9,00092	FLS 143
DO 01653 I#1,NP		FLS 144
01653	WRITE OUTPUT TAPE 9,(00093,I,P(I)),KI(I)	FLS 145
C	START LOOP TO PERFORM NC CYCLES AND ONE FINAL CALCULATION OF Y	FLS 146
NCY#NC+1		FLS 147
DO 01850 I#1,NCY		FLS 148
C	CLEAR ARRAYS AM AND V EXCEPT ON LAST CYCLE	FLS 149
IF(10-NCY)01851,02001,02001		FLS 150
01851	DO 01852 I#1,NM	FLS 151
01852	AM(I)=0.0	FLS 152
	DO 01902 I#1,NV	FLS 153
01902	V(I)=0.0	FLS 154
C	INITIALIZE FOR CYCLE 10 AND PUT OUT CAPTION FOR LIST OF Y(CALC)	FLS 155
02001	SQSIG(2)#SQSIG(1)	FLS 156
	SIG#0.0	FLS 157
	RNUM#0.0	FLS 158
	RZNUM#0.0	FLS 159
	RZDEN#0.0	FLS 160
	WRNUM#0.0	FLS 161
	WRZNUM#0.0	FLS 162
		FLS 163
		FLS 164
		FLS 165
		FLS 166
		FLS 167
		FLS 168
		FLS 169
		FLS 170
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		FLS 175
		FLS 176
		FLS 177
		FLS 178
		FLS 179
		FLS 180

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WRZDEN#0.0 FLS 181
WRITE OUTPUT TAPE 9,C0052,{TITLE(I),I#1,I2} FLS 182
WRITE OUTPUT TAPE 9,C0072,IC FLS 183
WRITE OUTPUT TAPE 9,C0073 FLS 184
FLS 185
C START LOOP THROUGH NO OBSERVATIONS FLS 186
02201 DO 05101 I#1,NO FLS 187
FLS 188
C ENTER SUBROUTINE CALC TO COMPUTE Y(CALC) AND DERIVATIVES FLS 189
CALL CALC(X(I),I),YC,P,DC) FLS 190
FLS 191
C OBTAIN WEIGHT AND CALCULATE QUANTITIES FROM Y(OBS)-Y(CALC) FLS 192
IF(IW)02601,C2501,02601 FLS 193
FLS 194
02501 SQRTW#1.0/SIGYC(I) FLS 195
GO TO 02701 FLS 196
FLS 197
02601 SIGYC(I)#1.0 FLS 198
SQRTW#1.0 FLS 199
FLS 200
02701 DY#YC(I)-YC FLS 201
WDY#SQRTW#DY FLS 202
SIG#SIG+WDY*WDY FLS 203
RZNUM#RZNUM+ABSF(DY) FLS 204
RZDEN#RZDEN+ABSF(YO(I)) FLS 205
WRZNUM#WRZNUM+WDY**2 FLS 206
WRZDEN#WRZDEN+(SORTW*YC(I))**2 FLS 207
IF(YO(I))02752,02801,02752 FLS 208
FLS 209
02752 RNUM#RNUM+ABSF(DY) FLS 210
WRNUM#WRNUM+KCY**2 FLS 211
FLS 212
C PUT OUT Y(CALC) AND OTHER INFORMATION FOR ONE OBSERVATION FLS 213
02801 DO 02802 K#1,4 FLS 214
FLS 215
02802 IHKL(K)#X(K,I) FLS 216
FLS 217
WRITE OUTPUT TAPE 9,C0079,(IHKL(K),K#1,3),YC(I),YC,A,B,DY, FLS 218
SIGYC(I),WDY,IHKL(4) FLS 219
FLS 220
C BY-PASS DERIVATIVE AND MATRIX SET-UP ON FINAL CALC OF Y FLS 221
IF(IC-NCY)03001,C5101,C5101 FLS 222
FLS 223
C START LOOP TO STORE AN ARRAY OF NV DERIVATIVES FLS 224
03001 J#1 FLS 225
DO 04101 K#1,NP FLS 226
FLS 227
IF(KI(K))04101,04101,03301 FLS 228
FLS 229
03301 OV(J)#SQRTW*DC(K) FLS 230
FLS 231
04001 J#J+1 FLS 232
04101 CONTINUE FLS 233
C END LOOP TO OBTAIN DERIVATIVES FLS 234
FLS 235
C START LOOP TO STORE MATRIX AND VECTOR. SEE GLOSSARY FOR FLS 236
STORAGE SCHEME FLS 237
C JK#NM FLS 238
DO 05001 JK#1,NV FLS 239
FLS 240

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04301	IF(DV(J))04501,C44C1,C45C1	FLS 241
C	BY-PASS IF DERIVATIVE IS ZERO	FLS 242
04401	JK#JK-NV+J-1	FLS 243
	GO TO 05001	FLS 244
		FLS 245
04501	DO 04801 K#J,NV	FLS 246
	AM(JK)#AM(JK)+DV(J)*DV(K)	FLS 247
	JK#JK-1	FLS 248
04801	CONTINUE	FLS 249
	V(J)#V(J)+DV(J)*WDY	FLS 250
05001	CONTINUE	FLS 251
C	END LCOP TO STORE MATRIX AND VECTOR	FLS 252
		FLS 253
05101	CONTINUE	FLS 254
C	END LCOP THROUGH NO OBSERVATIONS	FLS 255
		FLS 256
C	COMPUTE AND PUT OUT AGREEMENT FACTORS	FLS 257
	SQSIG(1)#SQRTE(SIG/FLOAT(N0-NV))	FLS 258
	WRITE OUTPUT TAPE 9,C008L,IC,SIG,SQSIG(1)	FLS 259
	WRNUM#SQRTE(WRNUM)	FLS 260
	WRZNUM#SQRTE(WRZNUM)	FLS 261
	WRZDEN#SQRTE(WRZDEN)	FLS 262
	R#RNUM/RZDEN	FLS 263
	RZRZNIN/RZDEN	FLS 264
	WR#WRNUM/WRZDEN	FLS 265
	WR#WRZNUM/WRZDEN	FLS 266
	WRZ#WRZNUM/WRZDEN	FLS 267
	WR#WRZNUM/WRZDEN	FLS 268
	WRZ#WRZNUM/WRZDEN	FLS 269
	WRITE OUTPUT TAPE 9,C0041	FLS 270
	WRITE OUTPUT TAPE 9,C0042,RZNUM,RZDEN,RZ	FLS 271
	WRITE OUTPUT TAPE 9,C0043,RNUM,RZDEN,R	FLS 272
	WRITE OUTPUT TAPE 9,C0044,WRZNUM,WRZDEN,WRZ	FLS 273
	WRITE OUTPUT TAPE 9,C0046,WRNUM,WRZDEN,WR	FLS 274
		FLS 275
C	BY-PASS MATRIX INVERSION AND PARAMETER OUTPUT ON FINAL CYCLE	FLS 276
	IF(IC-NCY)054C1,087C1,08701	FLS 277
		FLS 278
C	START LOOP TO TEST FOR ZERO DIAGONAL ELEMENT	FLS 279
054C1	ISING#0	FLS 280
	I#NM	FLS 281
	IID#NV	FLS 282
	DO 05801 I#I,NV	FLS 283
		FLS 284
	IF(AM(I))C5701,C56C1,C5701	FLS 285
05601	ISING#1	FLS 286
	WRITE OUTPUT TAPE 9,C0083,1	FLS 287
		FLS 288
05701	I#I-IID	FLS 289
	IID#IID-	FLS 290
05801	CONTINUE	FLS 291
C	END LCOP TO TEST FOR ZERO DIAGONAL ELEMENT	FLS 292
		FLS 293
C	TERMINATE JOB IF ZERO DIAGONAL ELEMENT WAS FOUND	FLS 294
	IF(ISING)11501,C6C01,115C1	FLS 295
		FLS 296
C	ENTER SUBROUTINE TO REPLACE MATRIX WITH INVERSE	FLS 297
06001	CALL SMI(AM(NM),NV,ISING)	FLS 298
	IF(ISING)06201,063C1,C6201	FLS 299
		FLS 300

C		TERMINATE JOB IF SINGULAR MATRIX WAS FOUND	FLS 301
C6201		WRITE OUTPUT TAPE 9,CC0085	FLS 302
		GO TO 11501	FLS 303
C		START LOOP FOR MATRIX VECTOR MULTIPLICATION FOR	FLS 304
C		PARAMETER CHANGES	FLS 305
C6301	DO 07201 I#1,NV		FLS 306
	PCI#D.0		FLS 307
	IJ#NM-I+1		FLS 308
	IJD#NV-1		FLS 309
	CO 07001 J#1,NV		FLS 310
	PCI#PCI+AM(IJ)*V(J)		FLS 311
	IF(J-1)C6701,C6801,C6901		FLS 312
06701	IJ#IJ-IJD		FLS 313
	IJD#IJ-1		FLS 314
	GO TO E7E01		FLS 315
C	SAVE DIAGONAL ELEMENTS OF INVERSE MATRIX		FLS 316
C6801	DIAG(I)#AM(IJ)		FLS 317
06901	IJ#IJ-1		FLS 318
07001	CONTINUE		FLS 319
	PCI(I)#PCI		FLS 320
	SIG#SIG-PCI*V(I)		FLS 321
07201	CONTINUE		FLS 322
C	END LOOP FOR MATRIX VECTOR MULTIPLICATION		FLS 323
C	RECOMPUTE AGREEMENT FACTOR USING MODIFIED SIG		FLS 324
	SQSIG(I)#SQRT(SIG/FLOAT(NC-NV))		FLS 325
C	PUT OUT CAPTION FOR LIST OF CORRECTED PARAMETERS		FLS 326
	WRITE OUTPUT TAPE 9,CCC52,(TITLE(I),I#1,I2)		FLS 327
	WRITE OUTPUT TAPE 9,00086,IC		FLS 328
C	START LOOP TO CORRECT AND PUT OUT PARAMETERS		FLS 329
	J#1		FLS 330
	N#1		FLS 331
	DO 08001 I#1,NP		FLS 332
C	SET K TO SELECT APPROPRIATE LABEL		FLS 333
	IF(I-NQ-1)07452,07454,07456		FLS 334
07452	K#1		FLS 335
	GO TO 075C1		FLS 336
07454	K#2		FLS 337
	GO TO 075C1		FLS 338
07456	IF(ITF-I)C7457,07457,C7461		FLS 339
07457	K#XMDFLI-NQ-2,b)+3		FLS 340
	IF(K-8)07462,07459,07459		FLS 341
07459	K#14		FLS 342
	GO TO 07501		FLS 343
			FLS 344
			FLS 345
			FLS 346
			FLS 347
			FLS 348
			FLS 349
			FLS 350
			FLS 351
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			FLS 354
			FLS 355
			FLS 356
			FLS 357
			FLS 358
			FLS 359
			FLS 360

07461	K#XMODF(I-NQ-2,1)+3	FLS 361
07462	IF(K-3)C7501,07463,07501	FLS 362
07463	WRITE OUTPUT TAPE 9,00078,ATOM(N)	FLS 363
	N#N+1	FLS 364
C	TEST KEY INTEGERS	FLS 365
07501	IF(KI(I))C7601,07601,C7701	FLS 366
07601	1 WRITE OUTPUT TAPE 9,00088,(LABEL(L,K),L#I,2), P(I),P(I)	FLS 367
	GO TO 08001	FLS 368
07701	POLD#P(I) P(I)#POLD+PD(J) SIGP#SQRTF(DIAG(J))*SQSIG(I)	FLS 369
	WRITE OUTPUT TAPE 9,00089,(LABEL(L,K),L#I,2), POLD,PD(J),P(I),SIGP	FLS 370
	J#J+1	FLS 371
08001	CONTINUE	FLS 372
C	END LOOP TO CORRECT AND PUT OUT PARAMETERS	FLS 373
C	PUT OUT ESTIMATED AGREEMENT FACTORS	FLS 374
	WRITE OUTPUT TAPE 9,C0081,IC,SIG,SQSIG(I)	FLS 375
C	ENTER SUBROUTINE TO TEST PARAMETERS	FLS 376
	ISTOP#0	FLS 377
	CALL TEST	FLS 378
C	WRITE CORRECTED PARAMETERS ON AUXILIARY TAPE IF DESIRED	FLS 379
08201	IF(IT)C8202,08301,08202	FLS 380
08202	NT#IT+4 NPCD#8*((NQ-1)/8+1) WRITE OUTPUT TAPE NT,00031,(SC(I),I#1,NPCD) WRITE OUTPUT TAPE NT,00032,T0 DO 08202 I#1,NA	FLS 381
	WRITE OUTPUT TAPE NT,00033,ATOM(I),SF(I),AI(I), (XYZ(K,I),K#I,3)	FLS 382
08209	1 WRITE OUTPUT TAPE NT,00034,(BETA(K,I),K#I,6)	FLS 383
C	TERM[NATE JOB IF INDICATED BY USERS SUBROUTINE TEST	FLS 384
08301	IF(ISTOP)08401,08501,08401	FLS 385
08401	WRITE OUTPUT TAPE 9,00090,ISTOP GO TO 08701	FLS 386
08501	CONTINUE	FLS 387
C	END LOOP THROUGH NC CYCLES AND FINAL CALC OF Y	FLS 388
C	TERMINATE JOB	FLS 389
08701	IF(NC)11701,11701,08801	FLS 390
C	CALCULATE AND PUT OUT CORRELATION MATRIX	FLS 391
08801	WRITE OUTPUT TAPE 9,00052,(TITLE(I),I#1,12)	FLS 392
		FLS 393
		FLS 394
		FLS 395
		FLS 396
		FLS 397
		FLS 398
		FLS 399
		FLS 400
		FLS 401
		FLS 402
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		FLS 417
		FLS 418
		FLS 419
		FLS 420

WRITE OUTPUT TAPE 9,CCC97  
 DO 09101 I#,NV  
 DIAG(I)#I.C/SQRTF(DIAG(I))  
 09101 CONTINUE  
 IJ#NM  
 DO 10201 I#,NV  
 DO 09601 J#I,NV  
 ROW(J)#D.G  
 09601 CONTINUE  
 DO 10001 J#I,NV  
 ROW(J)#AM(LJ)\*DIAG(I)\*DIAG(J)  
 IJ#IJ-1  
 10001 CONTINUE  
 WRITE OUTPUT TAPE 9,CCC98,I,(RGW(J),J#I,NV)  
 10201 CONTINUE  
 C WRITE DATA REQUIRED FOR FUNCTION AND ERROR PROGRAM  
 10501 IF(IXFE)10601,11501,106C1  
 10601 WRITE OUTPUT TAPE 3,CCC53,ITF,NQ,NP  
 WRITE OUTPUT TAPE 3,CCC71,(P(I),I#I,NP)  
 WRITE OUTPUT TAPE 3,CCC7C,(K1(I),I#I,NP)  
 WRITE OUTPUT TAPE 3,CCC53,NV  
 VARI#SQSIG()\*\*2  
 CC 10703 I#,NM  
 10703 AM(I)#AM(I)\*VARI  
 K#N#Y/2  
 L#NM  
 DO 11201 I#,K  
 HOLD#AM(I)  
 AM(I)#AM(L)  
 AM(L)#HOLD  
 L#L-1  
 11201 CONTINUE  
 WRITE OUTPUT TAPE 3,CCC99,(AM(I),I#,NM)  
 END FILE 3  
 11501 IF(IT-I)(11701,11601,117C1)  
 11601 END FILE 5  
 11701 CALL EXIT  
 END

\*TYPE(FORTRAN)  
 C OR FLS, FORTRAN CRYSTALLOGRAPHIC LEAST SQUARES  
 C READ CRYSTAL STRUCTURE DATA AND STORE PARAMETERS

FLS 475  
 FLS 476  
 FLS 477

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SUBROUTINE PRELIM                                FLS 478
                                                FLS 479
                                                FLS 480
COMMON NC,NV,NX,IW,IP,IT,NP,ISENT,NO,NM,NCY,IC,SIG,YC   FLS 481
COMMON SQRTH,DY,WDY,JK,ISING,II,LID,PGI,IJ,IJD,POLD   FLS 482
COMMON SIGP,ISTOP,NT,NPCD,IXFE,HOLD,VARI   FLS 483
COMMON TITLE,P,X,Y,O,SIGYO,KI,SOSIG,AM,V,DC,DV,DIAG,PD,ROW   FLS 484
COMMON RNUM,RZNUM,RZCEN,WRNUM,WRZNUM,WRZDEN,R,RZ,WR,WRZ   FLS 485
COMMON LABEL,ATOM,IHKL   FLS 486
COMMON IFSQ,ITF,NF,NA,ICENT,NS,NQ,TU,TJ,HX,HHB,EXPIJ,COSIJ,SINIJ   FLS 487
COMMON FI,A,B,RHO,SINTHL,PT,IPT,FRACPT,FTA,FTACOS,FTASIN,TFI,PIFI   FLS 488
COMMON IC,SOTO,SQRTAB,F,DFDFTO   FLS 489
COMMON SC,SF,AI,XYZ,BETA,DADFI,DADAI,DADX,DBDX,DADB   FLS 490
COMMON DBDB,DFDS,DFDFI,DFDAI,DFDX,DFDB,TS,IS,HJ,HHJ,RCP,FX,PRCP   FLS 491
COMMON CA,CB   FLS 492
FLS 493
C DIMENSIONS FOR NV(MAX)#100,NP(MAX)#230,NO(MAX)#2500,NX(MAX)#4,   FLS 494
C NF(MAX)#10,NA(MAX)#20,NS(MAX)#24,NQ(MAX)#9   FLS 495
C DIMENSION TITLE(12),P(230),X(4,2500),Y(2500),SIGYO(2500),KI(230)   FLS 496
C DIMENSION SCSIG(2),AM(5150),VI(100),DC(230),DV(100)   FLS 497
C DIMENSION DIAG(100),PD(100),ROW(100),ATOM(20),LABEL(2,14),IHKL(4)   FLS 498
C DIMENSION SCI(9),SF(20),AT(20),XYZ(3,20),BETA(6,20),DADFI(20)   FLS 499
C DIMENSION DDFI(20),DADAI(20),DRAOI(20),DAOX(3,20),DBDX(3,20)   FLS 500
C DIMENSION DADB(6,20),DBCB(6,20),DFDS(9),DFDF(20),DFDAI(20)   FLS 501
C DIMENSION DFDX(3,20),DFDB(6,20),TS(2,3,24),IS(2,3,24),HJ(3),H(4)   FLS 502
C DIMENSION HHJ(6),RCP(6),FX(32,10),PRCP(6)   FLS 503
FLS 504
C READ AND PUT OUT CONTROL INFORMATION   FLS 505
READ INPUT TAPE 10,2,IFSQ,ITF,NF,NA,ICENT,NS,NQ   FLS 506
2 FORMAT (7I3)   FLS 507
IF(IFSQ-1)4,4,7   FLS 508
FLS 509
4 WRITE OUTPUT TAPE 9,5   FLS 510
5 FORMAT (1IHOBASED ON F)   FLS 511
GO TO 9   FLS 512
FLS 513
7 WRITE OUTPUT TAPE 9,8   FLS 514
8 FORMAT (19HOBASED ON F SQUARED)   FLS 515
FLS 516
9 IF(ITF-2)10,13,16   FLS 517
FLS 518
10 WRITE OUTPUT TAPE 9,11   FLS 519
11 FORMAT (30H1ISOTROPIC TEMPERATURE FACTORS)   FLS 520
GO TO 19   FLS 521
FLS 522
13 WRITE OUTPUT TAPE 9,14   FLS 523
14 FORMAT (32HCANISOTROPIC TEMPERATURE FACTORS)   FLS 524
GO TO 19   FLS 525
FLS 526
16 WRITE OUTPUT TAPE 9,17   FLS 527
17 FORMAT (43HUISOTROPIC TEMPERATURE FACTORS CONVERTED TO,   FLS 528
1     28H ANISOTROPIC BEFORE REFINING)   FLS 529
FLS 530
19 WRITE OUTPUT TAPE 9,20,NF   FLS 531
20 FORMAT (38HNUMBER OF SCATTERING FACTOR TABLES IS 13)   FLS 532
WRITE OUTPUT TAPE 9,22,NA   FLS 533
22 FORMAT (38HNUMBER OF ATOMS IN ASYMMETRIC UNIT IS 13)   FLS 534
IF(ICFNT-1)24,24,27   FLS 535
FLS 536
24 WRITE OUTPUT TAPE 9,25   FLS 537

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25	FORMAT (16HCENTROSYMMETRIC)	FLS 538
	GO TO 29	FLS 539
27	WRITE OUTPUT TAPE 9,28	FLS 540
28	FCRMAF (20HONCN-CENTROSYMMETRIC)	FLS 541
29	WRITE OUTPUT TAPE 9,30,NS	FLS 542
30	FORMAT (28HONNUMBER OF SYMMETRY CARDS IS I3)	FLS 543
	WRITE OUTPUT TAPE 9,32,NQ	FLS 544
32	FORMAT (27HONNUMBER OF SCALE FACTORS IS I3)	FLS 545
C	READ AND PUT OUT SCATTERING FACTOR TABLES	FLS 546
	IF(NF)4C,60,40	FLS 547
40	READ INPUT TAPE 10,50,({FX(I,J),I#1,32),J#1,NF)	FLS 548
50	FORMAT (8F9.3)	FLS 549
	DO 56 J#1,NF	FLS 550
	WRITE OUTPUT TAPE 9,55,J	FLS 551
55	FORMAT (24H0SCATTERING FACTOR TABLEI3/IH )	FLS 552
56	WRITE OUTPUT TAPE 9,57,{FX(I,J),I#1,32)	FLS 553
57	FCRMAF (1H 8F12.3)	FLS 554
C	READ AND PUT OUT SYMMETRY TRANSFORMATIONS	FLS 555
60	READ INPUT TAPE 10,70,((TS(I,J),(IS(K,I,J),K#1,2),I#1,3),J#1),NS)	FLS 556
70	FORMAT (F11.6,2I2,F11.6,2I2,F11.6,2I2)	FLS 557
	WRITE OUTPUT TAPE 9,74	FLS 558
74	FORMAT (2IH0SYMMETRY INFORMATION/67HE       TRANSFORMED X	FLS 559
	ITRANSFORMED Y                           TRANSFORMED Z/IH )	FLS 560
	WRITE OUTPUT TAPE 9,76,((TS(I,J),(IS(K,I,J),K#1,2),I#1,3),J#1),NS)	FLS 561
76	FORMAT (1H F13.6,2I2,F20.6,2I2,F20.6,2I2)	FLS 562
C	READ AND PUT OUT RECIPROCAL CELL PARAMETERS	FLS 563
	READ INPUT TAPE 10,90,(RCP(K),K#1,6)	FLS 564
90	FORMAT (6F9.6)	FLS 565
	WRITE OUTPUT TAPE 9,94,(RCP(K),K#1,6)	FLS 566
94	FORMAT (29H0RECIPROCAL CELL PARAMETERS  6F11.6)	FLS 567
	PRCP(1)*RCP(1)**2*.25	FLS 568
	PRCP(2)*RCP(2)**2*.25	FLS 569
	PRCP(3)*RCP(3)**2*.25	FLS 570
	PRCP(4)*RCP(4)*RCP(2)*RCP(6)*.25	FLS 571
	PRCP(5)*RCP(5)*RCP(3)*RCP(5)*.25	FLS 572
	PRCP(6)*RCP(6)*RCP(2)*RCP(3)*RCP(4)*.25	FLS 573
C	SET TAPE NUMBER FOR PARAMETER INPUT	FLS 574
	IF(IP)130,140,130	FLS 575
130	NT#4	FLS 576
	REWIND 4	FLS 577
	GO TO 150	FLS 578
140	NT#10	FLS 579
	IP#1	FLS 580
C	START LOOP TO READ PARAMETERS UNTIL DESIRED SET	FLS 581
	HAS BEEN READ	FLS 582
150	DO 190 J#1,IP	FLS 583
	READ INPUT TAPE NT,170,(SC(I),I#1,NQ)	FLS 584
170	FORMAT (8F9.6)	FLS 585
		FLS 586
		FLS 587
		FLS 588
		FLS 589
		FLS 590
		FLS 591
C	START LOOP TO READ PARAMETERS UNTIL DESIRED SET	FLS 592
	HAS BEEN READ	FLS 593
150	DO 190 J#1,IP	FLS 594
	READ INPUT TAPE NT,170,(SC(I),I#1,NQ)	FLS 595
170	FORMAT (8F9.6)	FLS 596
		FLS 597

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      READ INPUT TAPE NT,170,Y0          FLS 578
      DO 190 I#1,NA                      FLS 599
      FLS 600
      READ INPUT TAPE NT,200,ATOM(I),SF(I),AI(I),(XYZ(K,I),K#1,3) FLS 601
      190  READ INPUT TAPE NT,210,IBETA(K,I),K#1,6)                  FLS 602
      200  FORMAT (A6,3X,SF9.6)                   FLS 603
      210  FORMAT (6F9.6)                     FLS 604
      FLS 605
      C   CONVERT ISOTROPIC TEMPRATURE FACTOR TO ANISOTROPIC IF SPECIFIED FLS 606
      IF (ITF#3)280,230,280                 FLS 607
      FLS 608
      230  DO 260 I#:NA                    FLS 609
      TFI#BETA(I,I)
      DO 260 K#1,6                         FLS 610
      FLS 611
      FLS 612
      FLS 613
      260      BETA(K,I)*TFI*PRCP(K)       FLS 614
      FLS 615
      270      ITF#2                      FLS 616
      FLS 617
      C   COMPUTE THE TOTAL NUMBER OF PARAMETERS FLS 618
      280  IF(ITF#1)310,290,310           FLS 619
      FLS 620
      290  NP#6*NA+NQ+1                  FLS 621
      GC TC 320                           FLS 622
      FLS 623
      310  NP#I#NA+NQ+1                  FLS 624
      FLS 625
      C   COPY PARAMETERS INTO THE ARRAY P FLS 626
      320 CALL SBTOP(P,SC,TO,SF,AI,XYZ,BETA,ITF,NA,NQ,np)    FLS 627
      RETURN                                FLS 628
      END                                    FLS 629

      *TYPE(FORTRAN)
      C   OR FLS, FORTRAN CRYSTALLOGRAPHIC LEAST SQUARES      FLS 630
      C   CALCULATE STRUCTURE FACTOR AND DERIVATIVES FOR ONE REFLECTION FLS 631
      FLS 632
      FLS 633
      SUBROUTINE CALC(H,Y,PAR,DER)          FLS 634
      FLS 635
      COMMON NC,NV,NX,IW,IP,IT,np,ISENT,NO,NM,NCY,IC,SIG,YC      FLS 636
      COMMON SQRTk,DY,WDY,JK,ISING,II,ILD,PD1,IJ,IJD,POLO      FLS 637
      COMMON SIGP,ISTCP,NT,NPCD,IXFE,HOLD,VARI                 FLS 638
      COMMON TITLE,P,X,Y,O,SEGOY,K,SQSIG,AM,V,DC,DV,DIAG,PD,ROW  FLS 639
      COMMON RNUM,RZNUM,RZDEN,WRNUM,WRZNUM,WRZDEN,R,KZ,WR,KRZ   FLS 640
      COMMON LABEL,ATCM,IHKL                FLS 641
      COMMON IFSG,ITF,NF,NA,ICENT,NS,NQ,TO,TJ,HX,HHB,EXPIJ,COSIJ,SINIJ FLS 642
      COMMON FI,A,B,RHO,SINTHL,PT,IPt,FRACPT,FTA,FTACOS,FIASIN,TFI,PIFI FLS 643
      COMMON IC,SQTO,SQRTAB,F,DFDFO      FLS 644
      COMMON SC,SF,AI,XYZ,BETA,DADFI,DADAI,DBDAI,DADX,DBDX,UADB FLS 645
      COMMON DBDR,DFDS,DFDFI,CFDAI,DFDX,DFCH,TS,IS,HJ,HHJ,RCP,FX,PRCP FLS 646
      COMMON CA,GB                          FLS 647
      FLS 648
      C   DIMENSIONS FOR NV(MAX)#100,NP(MAX)#230,NO(MAX)#2500,NX(MAX)#4,   FLS 649
      C   NF(MAX)#10,NA(MAX)#20,NS(MAX)#24,NQ(MAX)#9            FLS 650
      DIMENSION TITLE(12),P(230),X(4,2500),Y(2500),SIGY0(2500),KI(230) FLS 651
      DIMENSION SC(SIG(12),AM(5150),VI(100),CC(230),DV(100))      FLS 652
      DIMENSION DIAG(100),PD(100),ROW(100),ATOM(120),LABEL(2,14),IHKL(4) FLS 653
      DIMENSION SC( 9),SF(20),AI(20),XYZ(3,20),BETA(6,20),DADFI(20)  FLS 654

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DIMENSION DBDFI(20),DADAI(20),DBDAI(20),DADX(3,20),CBOX(3,20) FLS 655
DIMENSION DADB(6,20),DRCB(6,20),DFDS( 9),DFDF1(20),CFDAI(20) FLS 656
DIMENSION DFDX(3,20),DFCB(6,20),TS(3,24),IS(2,3,24),HJ(3),H(4) FLS 657
DIMENSION HHJ(6),RCP(6),FX(32,10),PRCP(6) FLS 658
FLS 659

C      COMPUTE REQUIRED SUMS OVER NS SYMMETRY TRANSFORMATIONS FLS 660
C      FOR EACH OF NA ATOMS FLS 661
C      CLEAR STORAGE ARRAYS FLS 662
DO 109 I#1,NA FLS 663
FLS 664
FACFI(I)#0.0 FLS 665
CBDFI(I)#0.0 FLS 666
DO 106 K#1,3 FLS 667
FLS 668
DADX(K,I)#0.0 FLS 669
DBDX(K,I)#0.0 FLS 670
DO 109 K#1,6 FLS 671
FLS 672
FLS 673
DADB(K,I)#0.0 FLS 674
DRCB(K,I)#0.0 FLS 675
FLS 676
FLS 677
FLS 678
FLS 679
C      START LOOP THROUGH THE NS SYMMETRY TRANSFORMATIONS FLS 679
DO 2301 J#1,NS FLS 679
FLS 680
C      STORE TRANSFORMED INDICES FLS 681
TJ#0.0 FLS 682
DO 316 I#1,3 FLS 683
FLS 684
TJ#TJ+H(I)*TS(I,J) FLS 685
HJ(I)#0.0 FLS 686
DO 315 K#1,3 FLS 687
FLS 688
KKKKK FLS 689
DO 314 L#1,2 FLS 690
LLLKL FLS 691
M#ISL,K,J FLS 692
IF(M-I)312,311,312 FLS 693
FLS 694
HJ(I)#HJ(I)+H(K) FLS 695
GO TO 314 FLS 696
FLS 697
312      IF(M+I)314,313,314 FLS 698
FLS 699
313      HJ(I)#HJ(I)-H(K) FLS 700
FLS 701
314      CONTINUE FLS 702
FLS 703
315      CONTINUE FLS 704
FLS 705
316      CONTINUE FLS 706
FLS 707
C      COMPUTE PRODUCTS OF TRANSFORMED INDICES FLS 708
FHJ(1)*HJ(1)**2 FLS 709
FHJ(2)*HJ(2)**2 FLS 710
FHJ(3)*HJ(3)**2 FLS 711
HHJ(4)*2.0*HJ(1)*HJ(2) FLS 712
HHJ(5)*2.0*HJ(1)*HJ(3) FLS 713
HHJ(6)*2.0*HJ(2)*HJ(3) FLS 714

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C	START LOOP THROUGH THE NA ATOMS	FLS 715
DO 2201 I#1,NA		FLS 716
		FLS 717
		FLS 718
C	ENTER USERS SUBROUTINE TO SET INDICES FOR SPECIAL POSITIONS	FLS 719
CALL PATCH(I,TJ,HJ,HHJ)		FLS 720
		FLS 721
C	COMPUTE TRIGONOMETRIC TERMS	FLS 722
HX#TJ		FLS 723
DO 803 K#1,3		FLS 724
		FLS 725
603	HX#HX+HJ(K)*XYZ(K,I)	FLS 726
		FLS 727
CCSIJ#COSF(6.2831853)*HX)		FLS 728
SINIJ#SINF(6.2831853)*HX)		FLS 729
		FLS 730
C	COMPUTE ANISOTROPIC TEMPERATURE FACTOR	FLS 731
IF(ITF-1)901,901,801		FLS 732
		FLS 733
801	HHB#0.0	FLS 734
DO 803 K#1,6		FLS 735
		FLS 736
803	HHB#HHB+HHJ(K)*BETA(K,I)	FLS 737
		FLS 738
EXPIJ#EXP(-HHB)		FLS 739
COSIJ#COSIJ#EXPIJ		FLS 740
SINIJ#SINIJ#EXPIJ		FLS 741
		FLS 742
C	ACCUMULATE REQUIRED SUMS	FLS 743
901	DADFI(I)#DADFI(I)+COSIJ	FLS 744
DO 1101 K#1,3		FLS 745
		FLS 746
1101	DADX(K,I)#DADX(K,I)+HJ(K)*SINIJ	FLS 747
		FLS 748
IF(ITF-1)(501,1501,1301		FLS 749
		FLS 750
1301	DO 1401 K#1,6	FLS 751
1401	DADB(K,I)#DADB(K,I)+HJ(K)*COSIJ	FLS 752
		FLS 753
C	HYPASS REMAINING SUMS IF CENTROSYMMETRIC	FLS 754
1501	IF(ICENT-1)2201,2201,1601	FLS 755
		FLS 756
1601	DBDFI(I)#DBDFI(I)+SINIJ	FLS 757
DO 1801 K#1,3		FLS 758
		FLS 759
1801	DBDX(K,I)#DBDX(K,I)+HJ(K)*COSIJ	FLS 760
		FLS 761
IF(ITF-1)2201,2201,2001		FLS 762
		FLS 763
2001	DO 2101 K#1,6	FLS 764
2101	DBDH(K,I)#DBDH(K,I)+HJ(K)*SINIJ	FLS 765
		FLS 766
2201	CONTINUE	FLS 767
C	END LOOP THROUGH THE NA ATOMS	FLS 768
2301	CONTINUE	FLS 769
C	END LOOP THROUGH THE NS SYMMETRY TRANSFORMATIONS	FLS 770
		FLS 771
		FLS 772
		FLS 773
		FLS 774

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C      COMPUTE A AND B AND THEIR DERIVATIVES          FLS  775
A#C.0
B#C.0
RHO#H(1)**2*PRCP(1)+H(2)**2*PRCP(2)+H(3)**2*PRCP(3)
1   +2.0*H(1)*H(2)*PRCP(4)+2.0*H(1)*H(3)*PRCP(5)
2   +2.0*H(2)*H(3)*PRCP(6)
IF(NF)270I,280I,27G1

270I   SINTHL#SQRTE(RHO)
PT#SINHL/.CS+I.C
IPT#PT
FRACPT#PT-FLOATF(IPT)

C      START LOOP THROUGH NA ATOMS          FLS  788
280I   DC 520I I#1,NA
FLS  789
FLS  790

C      OBTAIN SCATTERING FACTOR          FLS  791
IF(NF)31C1,300I,31C1
FLS  792
FLS  793

300I   FI#SF(I)
GO TO 320I
FLS  794
FLS  795
FLS  796

310I   L#SF(I)
FI#FX(IPT,L)+(FX(IPT+1,L)-FX(IPT,L))*FRACPT
FLS  797
FLS  798
FLS  799

C      COMPUTE ISOTROPIC TEMPERATURE FACTOR          FLS  800
320I   IF(IITF-1)340I,340I,330I
FLS  801
FLS  802

330I   TFT#I.C
GO TO 350I
FLS  803
FLS  804
FLS  805

340I   TFI#EXP(-BETA(I,I)*RHO)
FLS  806
FLS  807

C      COMPUTE A AND ITS DERIVATIVES          FLS  808
350I   FT#FI*TFL*A(I)
FTACOS#FTA*DADFI(I)
A#A+FTACOS
CACAI(I)#FI*I*CAF(I)
CAF(I)*A(I)*TFI*DADFI(I)
PIFI#-6.2831653I*FTA
CO 380I K#I,5
FLS  809
FLS  810
FLS  811
FLS  812
FLS  813
FLS  814
FLS  815
FLS  816
FLS  817
FLS  818
FLS  819
FLS  820

400I   DO 41C1 K#I,6
FLS  821
FLS  822
FLS  823
FLS  824
FLS  825
FLS  826
FLS  827
FLS  828
FLS  829
FLS  830
FLS  831
FLS  832
FLS  833
FLS  834

C      COMPUTE B AND ITS DERIVATIVES UNLESS CENTROSYMMETRIC
430I   IF(ICENT-1)520I,520I,440I
FTASIN#FTA*DADFI(I)
B#B+FTASIN
CBDA(I)#FI*I*TFI*DADFI(I)

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      DBCFI(I)*AI(I)*TFI*DRCFI(I)   FLS 835
      PIFI#-PIFL   FLS 836
      GO 4701 K#1,3   FLS 837
      FLS 838
      FLS 839
      FLS 840
      FLS 841
      FLS 842
      FLS 843
      FLS 844
      FLS 845
      FLS 846
      FLS 847
      FLS 848
      FLS 849
      FLS 850
      FLS 851
      FLS 852
      FLS 853
      FLS 854
      FLS 855
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      FLS 880
      FLS 881
      FLS 882
      FLS 883
      FLS 884
      FLS 885
      FLS 886
      FLS 887
      FLS 888
      FLS 889
      FLS 890
      FLS 891
      FLS 892

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          GO TO 6401                                FLS  893
6301      F#SQTO*(A**2+B**2)                      FLS  894
          CA#2.0*SQTO*A                          FLS  895
          CB#2.0*SQTO*B                          FLS  896
          FLS  897
          FLS  898
6401      DFCS(IQ)#2.0*F/SC(IQ)                  FLS  899
          DFOTO#-2.0*RHO*F                         FLS  900
          FLS  901
          FLS  902
          FLS  903
6501      Y#F                                     FLS  904
C       COMPUTE DERIVATIVES OF F OR F**2          FLS  905
C       START LOOP THROUGH NA ATOMS              FLS  906
          DO 7501 I#,NA
          FLS  907
          FLS  908
          FLS  909
          FLS  910
          FLS  911
          FLS  912
          FLS  913
          FLS  914
          FLS  915
          FLS  916
          FLS  917
          FLS  918
          FLS  919
          FLS  920
          FLS  921
          FLS  922
          FLS  923
          FLS  924
          FLS  925
C       COPY DERIVATIVES INTO ARRAY DER WHICH IS THE SAME AS DC   FLS  926
          CALL SBTOPICER,DFCS,DFETO,DFCFI,DFDAI,DFDX,DFDH,LTF,NA,NG,NP) FLS  927
          RETURN
          END                                         FLS  928
                                                 FLS  929

*TYPE(FORTRAN)
C       OR FLS, FORTRAN CRYSTALLOGRAPHIC LEAST SQUARES          FLS  930
C       TEST FOR NON-POSITIVE-DEFINITE TEMPERATURE FACTORS        FLS  931
          FLS  932
          FLS  933
          FLS  934
          FLS  935
          FLS  936
          FLS  937
          FLS  938
          FLS  939
          FLS  940
          FLS  941
          FLS  942
          FLS  943
          FLS  944
          FLS  945
          FLS  946
          FLS  947
          FLS  948

C       DIMENSIONS FOR NV(MAX)*100,NP(MAX)*230,NO(MAX)*2500,NX(MAX)*4,  FLS  948

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C      NF(MAX)#10,NA(MAX)#2C,NS(MAX)#24,NQ(MAX)#9          FLS  949
DIMENSION TITLE(12),P(230),X(4,2500),Y(2500),SIGYO(2500),KI(250) FLS  950
DIMENSION SOSIG(2),AP(15150),V(1C0),DC(230),DV1(E0)           FLS  951
DIMENSION DIAG(:00),PD(100),ROW(100),ATOM(120),LABEL(2,14),HKL(4) FLS  952
DIMENSION SC( 9),SF(20),A(120),XYZ(3,20),BETA(6,20),DADFI(20)   FLS  953
DIMENSION CRDFI(2C),CADA(120),CRDAI(20),DADX(3,25),CBX(3,2C)    FLS  954
DIMENSION DADFI(6,20),DBC(6,20),DFDS( 9),DFDFI(20),CFDAI(20)   FLS  955
DIMENSION DFDX(3,20),DFCR(6,20),TS(3,24),IS(2,3,24),HJ(3),H(4)  FLS  956
DIMENSION HHJ(6),RCP(6),FX(32,1C),PRCP(6)                      FLS  957
                                            FLS  958
C      STORE ADJUSTED PARAMETERS IN VARIOUS ARRAYS             FLS  959
CALL PTOSB(P,SC,TO,SF,AI,XYZ,BETA,ITF,NA,NQ,NP)            FLS  960
                                            FLS  961
C      ENTER USERS SUBROUTINE TO RESET SYMMETRY-RELATED COORDINATES FLS  962
CALL RESETX(XYZ)                                         FLS  963
                                            FLS  964
C      ENTER USERS SUBROUTINE TO RESET SYMMETRY-RELATED ANISOTROPIC FLS  965
TEMPERATURE FACTOR COEFFICIENTS                         FLS  966
C      IF(ITF-1)60,60,50                                     FLS  967
                                            FLS  968
50      CALL RESETB(BETA)                                    FLS  969
                                            FLS  970
C      START LCCP THROUGH NA ATOMS                         FLS  971
60  DO 220 I#1,NA                                       FLS  972
                                            FLS  973
80      IF(ITF-1)100,90,1C0                                FLS  974
                                            FLS  975
C      DISTRIBUTE OVERALL TEMPERATURE FACTOR AMONG ATOMS AND TEST FLS  976
90      BETA(1,1)*BETA(1,1)+TO                           FLS  977
         IF(BETA(1,1))190,220,220
                                            FLS  978
         IF(TO)110,130,110                                FLS  979
                                            FLS  980
                                            FLS  981
C      DISTRIBUTE OVERALL TEMPERATURE FACTOR AMONG BETAS        FLS  982
110     DO 120 K#1,6                                     FLS  983
         BETA(K,1)*BETA(K,1)+TO*PRCP(K)                  FLS  984
120     BETA(K,1)*BETA(K,1)+TO*PRCP(K)                  FLS  985
                                            FLS  986
C      TEST ANISOTROPIC TEMPERATURE FACTOR COEFFICIENTS       FLS  987
130     DC 145 K#1,3                                     FLS  988
         IF(BETA(K,1))190,145,145
         CONTINUE                                         FLS  989
140     IF(BETA(1,1)*BETA(2,1)-BETA(4,1)**2)190,160,160 FLS  990
145     IF(BETA(1,1)*BETA(3,1)-BETA(5,1)**2)190,170,170 FLS  991
150     IF(BETA(2,1)*BETA(3,1)-BETA(6,1)**2)190,180,180 FLS  992
155     IF(BETA(1,1)*BETA(2,1)*BETA(3,1)                 FLS  993
         +(BETA(4,1)*BETA(5,1)*BETA(6,1))*2.0          FLS  994
         -BETA(1,1)*BETA(6,1)**2-BETA(2,1)*BETA(5,1)**2  FLS  995
         -BETA(3,1)*BETA(4,1)**2)190,220,220          FLS  996
                                            FLS  997
                                            FLS  998
160     IF(BETA(1,1)*BETA(2,1)*BETA(3,1)                 FLS  999
         +(BETA(4,1)*BETA(5,1)*BETA(6,1))*2.0          FLS  1000
         -BETA(1,1)*BETA(6,1)**2-BETA(2,1)*BETA(5,1)**2  FLS  1001
         -BETA(3,1)*BETA(4,1)**2)190,220,220          FLS  1002
                                            FLS  1003
C      PUT OUT ERROR STATEMENT                         FLS  1004
190     WRITE OUTPUT TAPE 9,2C0,I                      FLS  1005
200     FORMAT(12PHOTEMPERATURE FACTOR OF ATOM I2,          FLS  1006
         25H IS NOT POSITIVE-DEFINITE)                  FLS  1007
         ISTOP#1                                         FLS  1008

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      220  CCNTINUE          FLS 1009
C      END LOOP THROUGH NA ATOMS          FLS 1010
C      TO #C.D          FLS 1011
C      COPY PARAMETERS INTO THE ARRAY P          FLS 1012
C      CALL SBTOP(P,SC,T0,SF,AI,XYZ,BETA,ITF,NA,NQ,NP)          FLS 1013
C      RETURN          FLS 1014
C      END          FLS 1015
C      FLS 1016
C      FLS 1017
C      FLS 1018

*TYPE(FORTRAN)          FLS 1019
C      OR FLS, FORTRAN CRYSTALLOGRAPHIC LEAST SQUARES          FLS 1020
C      COPY PARAMETERS FROM ARRAY P TO ARRAYS USED BY SUBROUTINES          FLS 1021
C      SUBROUTINE PTOSB(P,SC,TC,SF,AI,XYZ,BETA,ITF,NA,NQ,NP)          FLS 1022
C      DIMENSION P(230),SC( 9),SF(20),AI(20),XYZ(3,20),BETA(6,20)
C      TO I#1          FLS 1023
C      DO 40 J#1,NA          FLS 1024
C      SC(J)#P(I)          FLS 1025
C      40   I#I+1          FLS 1026
C      TC#P(I)
C      60   I#I+1          FLS 1027
C      70   DO 220 J#1,NA          FLS 1028
C      SF(J)#P(I)
C      90   AI(J)#P(I+1)          FLS 1029
C      100  I#I+2          FLS 1030
C      110  GO 130 K#1,3          FLS 1031
C      120   XYZ(K,J)#P(I)          FLS 1032
C      130   I#I+1          FLS 1033
C      140   IF(ITF-I)150,150,190          FLS 1034
C      150   BETA(I,J)#P(I)          FLS 1035
C      160   I#I+1          FLS 1036
C      170   GO TO 220          FLS 1037
C      190   DO 210 K#1,6          FLS 1038
C      200   BETA(K,J)#P(I)          FLS 1039
C      210   I#I+1          FLS 1040
C      220   CCNTINUE          FLS 1041
C      RETURN          FLS 1042
C      END          FLS 1043
C      FLS 1044
C      FLS 1045
C      BETA(I,J)#P(I)          FLS 1046
C      I#I+1          FLS 1047
C      GO TO 220          FLS 1048
C      DO 210 K#1,6          FLS 1049
C      BETA(K,J)#P(I)          FLS 1050
C      I#I+1          FLS 1051
C      DO 210 K#1,6          FLS 1052
C      BETA(K,J)#P(I)          FLS 1053
C      I#I+1          FLS 1054
C      220   CCNTINUE          FLS 1055
C      RETURN          FLS 1056
C      END          FLS 1057
C      FLS 1058

*TYPE(FCRTRAN)          FLS 1059
C      OR FLS, FORTRAN CRYSTALLOGRAPHIC LEAST SQUARES          FLS 1060
C      COPY PARAMETERS FROM ARRAYS USED BY SUBROUTINES TO ARRAY P          FLS 1061
C      FLS 1062

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SUBROUTINE SBTOP(P,SC,IC,SF,AI,XYZ,BETA,ITF,NA,NQ,NP)          FLS 1063
  DIMENSION P(230),SC( 9),SF(20),AI(20),XYZ(3,20),BETA(6,20)    FLS 1064
  FLS 1065
  FLS 1066
  FLS 1067
  FLS 1068
  FLS 1069
  FLS 1070
  FLS 1071
  FLS 1072
  FLS 1073
  FLS 1074
  FLS 1075
  FLS 1076
  FLS 1077
  FLS 1078
  FLS 1079
  FLS 1080
  FLS 1081
  FLS 1082
  FLS 1083
  FLS 1084
  FLS 1085
  FLS 1086
  FLS 1087
  FLS 1088
  FLS 1089
  FLS 1090
  FLS 1091
  FLS 1092
  FLS 1093
  FLS 1094
  FLS 1095
  FLS 1096
  FLS 1097
  FLS 1098

10  I#1
20  DO 40 J#1,NQ
30    P(I)#SC(J)
40    I#I+1
50  P(I)#TO
60  I#I+1
70  GO 220 J#1,NA
80    P(I)#SF(J)
90    P(I+1)#AI(J)
100   I#I+2
110   GO 130 K#1,3
120    P(I)#XYZ(K,J)
130    I#I+1
140  IF(I#F-I)150,150,190
150    P(I)#BETA(I,J)
160    I#I+1
170  GO TO 220
190    DC 210 K#1,6
200    P(I)#BETA(K,J)
210    I#I+1
220  CCNTINUE
      RETURN
      END

```

```

*TYPE(FAP)
  COUNT 230
  REM SYMMETRIC MATRIX INVERSE. SEE GLOSSARY FOR STORAGE SCHEME.
  REM FOR USE ON 704, 7C9, OR 7C90.
  REM WRITTEN IN FAP FOR ASSEMBLY ON 7D9 OR 7D90.
  ENTRY SMI
  SMI  SXD T13,1
  SMI  SXD T14,2
  LFTM
  TNC **1
  CAL 1,4
  COM
  PAX 0,2
  TXI **1,2,*1
  CLA 2,4
  STA Y1
  CLA 3,4
  STA Y28
  STA SING1
  CLA 0
  PDX 0,1
          ADD SET
OVERFLOW Toggles
  FLS 1099
  FLS 1100
  FLS 1101
  FLS 1102
  FLS 1103
  FLS 1104
  FLS 1105
  FLS 1106
  FLS 1107
  FLS 1108
  FLS 1109
  FLS 1110
  FLS 1111
  FLS 1112
  FLS 1113
  FLS 1114
  FLS 1115
  FLS 1116
  FLS 1117
  FLS 1118
  FLS 1119

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	STO Y27		FLS 1120
	SXD T1,4		FLS 1121
Y2	SXD Y25,1	Y2	FLS 1122
	SXD T2,1		FLS 1123
	SXD T3,2		FLS 1124
	STZ T4	Y3	FLS 1125
	STZ T5,		FLS 1126
	LXD T4,4		FLS 1127
Y4	SXD Y7,1	Y4	FLS 1128
	CLA 0,2	Y5	FLS 1129
	SSP		FLS 1130
	FSB T4		FLS 1131
	TMI Y7		FLS 1132
	CLA 0,2	Y6	FLS 1133
	SSP		FLS 1134
	STG T4		FLS 1135
	SXD T5,4		FLS 1136
Y7	TIX Y8,2,0	Y7 DEC SET Y4,DELTA	FLS 1137
	HTR Y8		FLS 1138
Y8	TNX Y10,1,1	Y8	FLS 1139
	TXI Y4,4,1	Y9	FLS 1140
Y10	CAL T3	Y10	FLS 1141
	ACC T2		FLS 1142
	PDX 0,4		FLS 1143
	CLA T5		FLS 1144
	STO 0,4		FLS 1145
	TSX X1,4	Y11	FLS 1146
	LXD T3,2	Y12	FLS 1147
	CLA 0,2		FLS 1148
	TZE SING		FLS 1149
	TMI SING		FLS 1150
	CLA FLONE	Y13	FLS 1151
	FDP 0,2		FLS 1152
	STQ 0,2		FLS 1153
	CLS 0,2		FLS 1154
	STO T6		FLS 1155
	CLA PON	Y14	FLS 1156
	SUB T3		FLS 1157
	ARS 18		FLS 1158
	STA Y16A		FLS 1159
	STA Y19A	SETS ADDRESSES AT M	FLS 1160
	CLA PON		FLS 1161
	SUB T3		FLS 1162
	ACC T2		FLS 1163
	ARS 18		FLS 1164
	STA Y16		FLS 1165
	STA Y19A	SETS ADDRESSES AT M+N	FLS 1166
	LXD T2,1		FLS 1167
	LXD T2,2		FLS 1168
	CLA T3		FLS 1169
	SUB T2		FLS 1170
	PCK 0,4		FLS 1171
Y15	TNX Y17,1,1	Y15	FLS 1172
Y16	LDD 0,1	Y16 ADD SET Y14,M+N	FLS 1173
	FMP T6		FLS 1174
	TNC Y16A		FLS 1175
	SXD T12,4		FLS 1176
	TSX CFL,4		FLS 1177
	LXD T12,4		FLS 1178
Y16A	STO 0,1	ADD SET Y14,M	FLS 1179

	TNX Y15,D,C	DEC FOR T1,C(14)	FLS 1180
Y17	TNX Y24,2,I		FLS 1181
	PDX D,2		FLS 1182
	PDX D,I		FLS 1183
Y19	LCL D,I	Y19 ADD SET Y14,M	FLS 1184
Y19A	FMP D,2	ADD SET Y14,M+N	FLS 1185
	TNO Y19B		FLS 1186
	SXD T12,4		FLS 1187
	TSX OFL,4		FLS 1188
	LXD T12,4		FLS 1189
Y19B	FAC D,4		FLS 1190
	TNC Y19C		FLS 1191
	SXC T12,4		FLS 1192
	TSX CFL,4		FLS 1193
	LXC T12,4		FLS 1194
Y19C	STO D,4		FLS 1195
	TXI Y2B,4,-1		FLS 1196
Y20	TNX Y17,I,1	Y20	FLS 1197
	TNX Y19,D,0		FLS 1198
Y24	LXD T3,2	Y24	FLS 1199
	LXD T2,I		FLS 1200
	TNX Y26,I,1		FLS 1201
Y25	TIK Y2,2,J	Y25 DEC SET Y2	FLS 1202
	HTR Y2		FLS 1203
Y26	TXI Y26A,I,1	Y26	FLS 1204
Y26A	SXD Y29,I		FLS 1205
Y27	TXL Y29,I,0	Y27 DEC SET Y1,0	FLS 1206
	LXD T1,4		FLS 1207
	LXD T13,I		FLS 1208
	LXD T14,2		FLS 1209
Y28	STZ D	ADD SET	FLS 1210
	EFTM		FLS 1211
	TRA I,4	NORMAL RETURN	FLS 1212
Y29	TXI Y29A,2,0	Y29 DEC SET Y26	FLS 1213
Y29A	SXD T3,2		FLS 1214
	SXD T2,I		FLS 1215
	CLA PON	Y30	FLS 1216
	SUB T3		FLS 1217
	ARS I8		FLS 1218
	STA Y35	SETS ADDRESSES	FLS 1219
	STA Y38	AT M	FLS 1220
	STA Y39		FLS 1221
	STA Y39B		FLS 1222
	STA Y39C		FLS 1223
	CLA PON		FLS 1224
	SUB T3		FLS 1225
	ADD T2		FLS 1226
	ARS I8		FLS 1227
	STA Y3I	SETS ADDRESSES	FLS 1228
	STA Y36	AT M+N	FLS 1229
	STA Y36A		FLS 1230
	STA Y38B		FLS 1231
	STA Y38C		FLS 1232
	STA Y39A		FLS 1233
	CLA T2		FLS 1234
	SUB ONE		FLS 1235
	PDX D,I	SETS INDEXES	FLS 1236
	PDX D,2	AT M-N	FLS 1237
Y31	STZ D,I	Y31 ADC SET Y30,M+N	FLS 1238
	TIK Y31,I,1	Y32	FLS 1239

	CLA T3	Y33	FLS 1240
	SUB T2		FLS 1241
	PDX 0,4		FLS 1242
Y34	PXD 0,2	Y34	FLS 1243
	PDX 0,1		FLS 1244
Y35	LCQ 0,2	Y35 ADD SET Y30,M	FLS 1245
	FMP 0,4		FLS 1246
	TNO Y36		FLS 1247
	SXD T12,4		FLS 1248
	TSX OFL,4		FLS 1249
	LXD T12,4		FLS 1250
Y36	FAC 0,1	Y36 ADD SET Y30,M+N	FLS 1251
	TNO Y36A		FLS 1252
	SXC T12,4		FLS 1253
	TSX OFL,4		FLS 1254
	LXD T12,4		FLS 1255
Y36A	STO 0,1	ADD SET Y30,M+N	FLS 1256
	TXI Y37,4,-1		FLS 1257
Y37	TNX Y39,1,1	Y37	FLS 1258
Y38	LCQ 0,1	Y38 ADD SET Y30,M	FLS 1259
	FMP 0,4		FLS 1260
	TNO Y38B		FLS 1261
	SXD T12,4		FLS 1262
	TSX OFL,4		FLS 1263
	LXD T12,4		FLS 1264
Y38B	FAD 0,2	ADD SET Y30,M+N	FLS 1265
	TNC Y38C		FLS 1266
	SXC T12,4		FLS 1267
	TSX OFL,4		FLS 1268
	LXD T12,4		FLS 1269
Y38C	STO 0,2	ADD SET Y30,M+N	FLS 1270
	TNX Y35,0,0		FLS 1271
Y39	LCQ 0,2	Y39 ADD SET Y30,M	FLS 1272
Y39A	FMP 0,2	ADD SET Y30,M+N	FLS 1273
	TNO Y39B		FLS 1274
	SXD T12,4		FLS 1275
	TSX OFL,4		FLS 1276
	LXD T12,4		FLS 1277
Y39B	FAC 0	ADD SET Y30,M	FLS 1278
	TNO Y39C		FLS 1279
	SXD T12,4		FLS 1280
	TSX OFL,4		FLS 1281
	LXD T12,4		FLS 1282
Y39C	STO 0	ADD SET Y30,M	FLS 1283
	TXI Y34,2,1	Y40 GO TO Y5C	FLS 1284
	CAL T3	Y50	FLS 1285
	ADD T2		FLS 1286
	PDX 0,4		FLS 1287
	CAL 0,4		FLS 1288
	SLW T5		FLS 1289
	TSX X1,4		FLS 1290
	LXD T3,2		FLS 1291
	LXD T2,1		FLS 1292
DT12	TNX Y26,0,0	DEC FOR T12	FLS 1293
SING	PXD 0,2	SINGULARITY RETURN	FLS 1294
	LXD T13,1		FLS 1295
	LXD T14,2		FLS 1296
	LXD T1,4		FLS 1297
	CLA ONE		FLS 1298
SING1	STO 0	ADD SET	FLS 1299

	EFTM		
OFL	TRA 4,4	ERROR RETURN	FLS 1300
	ARS I	OVERFLOW-UNDERFLOW	FLS 1301
	PBT		FLS 1302
DT13	TNX OFL+5,0,0	DEC FOR T13,C(I1)	FLS 1303
	PXD 0,0,0		FLS 1304
	TRA 1,4		FLS 1305
	PXD 0,4		FLS 1306
	SSM		FLS 1307
DT14	TNX SING+1,0,0	DEC FOR T14,C(I2)	FLS 1308
X1	CLA T5	X1	FLS 1309
	IZE 1,4		FLS 1310
	SXD T12,4	X2	FLS 1311
	LXD T2,1		FLS 1312
	LXD T3,2		FLS 1313
	CAL T3		FLS 1314
	SUB T5		FLS 1315
	PDX 0,4		FLS 1316
	STD X6		FLS 1317
X3	CAL 0,2	X3	FLS 1318
	LDQ 0,4		FLS 1319
	SLW 0,4		FLS 1320
	STQ 0,2		FLS 1321
	TNX X9,1,1	X4	FLS 1322
	SXD X8,1	X5	FLS 1323
X6	TXH X8,2,0	X6 DEC SET X2	FLS 1324
	CAL CNE	X7	FLS 1325
	STD X8		FLS 1326
X8	TIK X8A,4,0	X8 DEC SET X5,X7	FLS 1327
	HTR 0		FLS 1328
X8A	TXI X3,2,-1		FLS 1329
X9	LXD T3,2	X9	FLS 1330
	LXD X6,4		FLS 1331
	CAL 0,2		FLS 1332
	LDQ 0,4		FLS 1333
	SLW 0,4		FLS 1334
	STD 0,2		FLS 1335
	LXD T12,4	X10	FLS 1336
	TRA 1,4		FLS 1337
ONE	PZE 0,0,1	ONE	FLS 1338
FLCNE	DEC 1,0	FLONE	FLS 1339
PON	PCN 0,0,0	LGNO	FLS 1340
T2	PZE 0,0,0	T2, N	FLS 1341
T3	PZE 0,0,0	T3,-M	FLS 1342
T4	PZE 0,0,0	T4,X T6,-BII	FLS 1343
T5	PZE 0,0,0	T5,J	FLS 1344
T1	SYN DT1	C(I4)	FLS 1345
T6	SYN T4	-BII	FLS 1346
T12	SYN DT12	C(I4) FOR SR	FLS 1347
T13	SYN DT13	C(I1)	FLS 1348
T14	SYN DT14	C(I2)	FLS 1349
	END 0		FLS 1350
			FLS 1351

*TYPE(FORTRAN)	FLS 1352
C OR FLS, FORTRAN CRYSTALLOGRAPHIC LEAST SQUARES	FLS 1353
C DUMMY SUBROUTINE TO BE REPLACED BY USER IF NECESSARY	FLS 1354
SUBROUTINE PATCH(I,TJ,HJ,HNJ)	FLS 1355
	FLS 1356

```
      RETURN                               FLS 1357
      END                                 FLS 1358
```

```
*TYPE(FORTRAN)
C   OR FLS, FORTRAN CRYSTALLOGRAPHIC LEAST SQUARES
C   DUMMY SUBROUTINE TO BE REPLACED BY USER IF NECESSARY
      SUBROUTINE RESETX(XYZ)
      RETURN
      END                               FLS 1359
                                         FLS 1360
                                         FLS 1361
                                         FLS 1362
                                         FLS 1363
                                         FLS 1364
                                         FLS 1365
```

```
*TYPE(FORTRAN)
C   OR FLS, FORTRAN CRYSTALLOGRAPHIC LEAST SQUARES
C   DUMMY SUBROUTINE TO BE REPLACED BY USER IF NECESSARY
      SUBROUTINE RESETB(BETA)
      RETURN
      END                               FLS 1366
                                         FLS 1367
                                         FLS 1368
                                         FLS 1369
                                         FLS 1370
                                         FLS 1371
                                         FLS 1372
```

## SUBROUTINES FOR EXAMPLE

```
*TYPE(FORTRAN)
C   EXAMPLE. HYPOTHETICAL PROBLEM BASED ON ALPHA QUARTZ.
      SUBROUTINE PATCH(I,TJ,HJ,HHJ)
      DIMENSION HJ(3),HHJ(6)
      C   BY-PASS MODIFICATION FOR FIRST ATOM
      IF(I-1)2,2,
      1   HJ(1)=HJ(1)+HJ(2)
      HJ(2)=0.0
      HHJ(1)=HHJ(1)+HHJ(2)
      HHJ(2)=0.0
      HHJ(5)=HHJ(5)-HHJ(6)
      HHJ(6)=0.0
      2 RETURN
      END                               FLS 1373
                                         FLS 1374
                                         FLS 1375
                                         FLS 1376
                                         FLS 1377
                                         FLS 1378
                                         FLS 1379
                                         FLS 1380
                                         FLS 1381
                                         FLS 1382
                                         FLS 1383
                                         FLS 1384
                                         FLS 1385
                                         FLS 1386
                                         FLS 1387
                                         FLS 1388
                                         FLS 1389
```

```
*TYPE(FORTRAN)
C   EXAMPLE. HYPOTHETICAL PROBLEM BASED ON ALPHA QUARTZ.
      SUBROUTINE RESETX(XYZ)
      DIMENSION XYZ(3,2)
      XYZ(2,2)=XYZ(1,2)
      RETURN
      END                               FLS 1390
                                         FLS 1391
                                         FLS 1392
                                         FLS 1393
                                         FLS 1394
                                         FLS 1395
                                         FLS 1396
                                         FLS 1397
                                         FLS 1398
```

```
*TYPE(FORTRAN)
C   EXAMPLE. HYPOTHETICAL PROBLEM BASED ON ALPHA QUARTZ.
      SUBROUTINE RESETB(BETA)
                                         FLS 1399
                                         FLS 1400
                                         FLS 1401
```

```

DIMENSION BETA(6,2) FLS 1402
BETA(2,2)=BETA(1,2) FLS 1403
BETA(6,2)=BETA(5,2) FLS 1404
RETURN FLS 1405
END FLS 1406
FLS 1407
FLS 1408

```

### DATA FOR EXAMPLE

```

*DATA FLS 1409
SCALE FACTOROVERALL B FORM FACTOR MULTIPLIER X Y FLS 1410
Z BETA(1,1) BETA(2,2) BETA(3,3) BETA(1,2) BETA(1,3) FLS 1411
BETA(2,3) ATOMIC 8 FLS 1412
EXAMPLE. HYPOTHETICAL PROBLEM BASED ON ALPHA QUARTZ. FLS 1413
2 15 1 0 0 0 FLS 1414
2 3 2 2 2 6 1 FLS 1415
10.000 9.551 8.475 7.159 5.908 4.857 4.028 3.391 FLS 1416
2.916 2.568 2.287 2.106 1.929 1.812 1.714 1.637 FLS 1417
1.574 1.515 1.469 1.425 1.381 1.339 1.299 1.259 FLS 1418
1.220 1.179 1.143 1.105 1.068 1.033 0.997 0.966 FLS 1419
10.00 9.95 9.79 9.54 9.20 8.79 8.33 7.83 FLS 1420
7.31 6.78 6.26 5.77 5.28 4.85 4.42 4.06 FLS 1421
3.71 3.42 3.13 2.90 2.68 2.50 2.33 2.19 FLS 1422
2.06 1.96 1.86 0 0 0 0 0 FLS 1423
1 2 3 FLS 1424
1-2 -2 -3 FLS 1425
2-1 -1 0.33333333+3 FLS 1426
-1 2-1 0.33333333-3 FLS 1427
-2 1-2 0.66666667+3 FLS 1428
2 1 0.66666667-3 FLS 1429
0.23504 0.23504 0.18504 0 0 0.50000 FLS 1430
1.0 FLS 1431
0 FLS 1432
0 1. 1.0 0.4100 0.2700 0.1200 FLS 1433
0.38 FLS 1434
SI 2. 0.5 0.5200 0.5200 .3333333 FLS 1435
0.43 FLS 1436
1 0 0 234.6 1 FLS 1437
1 1 0 317.5 1 FLS 1438
6 1 0 76.0 1 FLS 1439
5 3 0 27.9 1 FLS 1440
4 0 1 308.2 1 FLS 1441
3 1 1 56.5 1 FLS 1442
3 2 1 1.5 1 FLS 1443
4 4 1 6.7 1 FLS 1444
3 1 -1 199.8 1 FLS 1445
5 2 -1 145.6 1 FLS 1446
2 0 2 78.7 1 FLS 1447
6 1 2 11.5 1 FLS 1448
5 3 2 38.0 1 FLS 1449
1 0 -2 80.3 1 FLS 1450
5 1 -2 45.2 1 FLS 1451
3 2 -2 9.0 1 FLS 1452
3 0 3 74.1 1 FLS 1453
2 2 3 212.0 1 FLS 1454
3 0 -3 12.5 1 FLS 1455
4 1 -3 231.3 1 FLS 1456
6 0 4 44.4 1 FLS 1457
6 2 4 32.0 1 FLS 1458

```

5	0	-4	180.2	)	FLS 1459
4	2	-4	33.3	)	FLS 1460
1	1	5	162.5	)	FLS 1461
3	0	-5	8.2	)	FLS 1462
2	2	6	85.9	)	FLS 1463
4	0	-6	110.5	)	FLS 1464
4	1	7	10.6	)	FLS 1465
1	1	-7	78.0	)	FLS 1466
3	0	8	134.9	)	FLS 1467
2	1	-8	37.2	)	FLS 1468
2	0	-9	10.8	)	FLS 1469
				)	FLS 1470
				)	FLS 1471

100011111111CC100101110

## PROGRAM OUTPUT FOR EXAMPLE

EXAMPLE. HYPOTHETICAL PROBLEM BASED ON ALPHA QUARTZ.

NUMBER OF CYCLES IN THIS JOB IS 2

NUMBER OF PARAMETERS TO BE VARIED IS 15

UNIT WEIGHTS TO BE SET BY PROGRAM

PARAMETERS TO BE READ AS INPUT DATA

CORRECTED PARAMETERS NOT TO BE SAVED FOR LATER USE

INPUT DATA FOR OR-FORTRAN FUNCTION AND ERROR PROGRAM NOT TO BE SAVED

BASED ON F SQUARED

ISOTROPIC TEMPERATURE FACTORS CONVERTED TO ANISOTROPIC BEFORE REFINING

NUMBER OF SCATTERING FACTOR TABLES IS 2

NUMBER OF ATOMS IN ASYMMETRIC UNIT IS 2

NON-CENTROSYMMETRIC

NUMBER OF SYMMETRY CARDS IS 6

NUMBER OF SCALE FACTORS IS 1

SCATTERING FACTOR TABLE 1

10.000	9.551	8.475	7.159	5.908	4.857	4.028	3.394
2.916	2.568	2.287	2.106	1.929	1.812	1.714	1.637
1.574	1.515	1.469	1.425	1.381	1.339	1.299	1.259
1.220	1.179	1.143	1.105	1.068	1.033	0.997	0.966

SCATTERING FACTOR TABLE 2

10.000	9.950	9.790	9.540	9.200	8.790	8.330	7.830
7.310	6.780	6.260	5.770	5.280	4.850	4.420	4.060
3.710	3.420	3.130	2.900	2.680	2.500	2.330	2.190
2.060	1.960	1.860	0.	0.	0.	0.	0.

SYMMETRY INFORMATION

TRANSFORMED X	TRANSFORMED Y	TRANSFORMED Z
---------------	---------------	---------------

-0.	1-0	-0.	2-0	-0.	3-0
-0.	1-2	-0.	-2-0	-0.	-3-0
-0.	2-1	-0.	-1-0	0.333333	3-0
-0.	-1-0	-0.	2-1	0.333333-3-0	
-0.	-2-0	-0.	1-2	0.666667	3-0
-0.	2-0	-0.	1-0	0.666667-3-0	

RECIPROCAL CELL PARAMETERS    0.235040    0.235040    0.185040    0.    0.    0.500000

NUMBER OF PARAMETERS READ IS 24

NUMBER OF OBSERVATIONS READ IS 33

INPUT DATA

I	P(I)	KI(I)
1	1.0000	1
2	0.	0
3	1.0000	0
4	1.0000	0
5	0.4100	1
6	0.2700	1
7	0.1200	1
8	0.0052	1
9	0.0052	1
10	0.0033	1
11	0.0026	1
12	0.	1
13	0.	1
14	2.0000	0
15	0.5000	0
16	0.5200	1
17	0.5200	0
18	0.3333	0
19	0.0059	1
20	0.0059	0
21	0.0037	1
22	0.0030	1
23	0.	1
24	0.	0

## EXAMPLE. HYPOTHETICAL PROBLEM BASED ON ALPHA QUARTZ.

## CALCULATED Y BASED ON PARAMETERS BEFORE CYCLE 1

H	K	L	Y(OBS)	Y(CALC)	A	B	OBS-CALC	SIG(0)	(C-C)/SIG(0)	IQ
1	0	0	234.6000	218.7436	-14.7900	-0.0000	15.8564	1.0000	15.8564	1
1	1	0	317.5000	407.2533	-17.1005	-10.7157	-89.7533	1.0000	-89.7533	1
6	1	0	76.0000	65.8654	-5.1086	-6.3062	10.1346	1.0000	10.1346	1
5	3	0	27.9000	13.7550	-1.5922	3.3496	14.1450	1.0000	14.1450	1
4	0	1	308.2000	201.8193	-7.032	-12.3030	106.3809	1.0000	106.3809	1
3	-1	1	56.5000	51.4033	-5.2238	4.9107	5.0967	1.0000	5.0967	1
3	2	1	1.5000	14.6171	-1.5141	-3.5106	-13.1171	1.0000	-13.1171	1
4	-1	1	6.7000	4.4200	-1.8372	1.0220	2.2800	1.0000	2.2800	1
3	1	-1	199.8000	240.7660	-11.9863	-9.8536	-40.9640	1.0000	-40.9640	1
5	2	-1	145.6000	148.1294	-6.3258	10.3978	-2.5294	1.0000	-2.5294	1
2	0	2	78.7000	78.5276	4.4308	-7.6744	0.1724	1.0000	0.1724	1
6	-1	2	11.5000	26.2909	4.6471	-1.6436	-12.7969	1.0000	-12.7969	1
5	3	2	38.0000	36.1223	0.7574	-5.9621	1.8797	1.0000	1.8797	1
1	0	-2	80.8000	69.5725	4.1705	7.2235	10.5275	1.0000	10.5275	1
5	1	-2	45.2000	59.9162	-3.8525	6.7137	-14.7162	1.0000	-14.7162	1
3	2	-2	9.0000	30.3347	-1.5870	-5.2739	-21.3347	1.0000	-21.3347	1
3	0	3	74.1000	90.0221	-9.1080	0.0000	-15.9221	1.0000	-15.9221	1
2	2	5	212.0000	252.9857	15.7640	2.1172	-40.9857	1.0000	-40.9857	1
3	0	-3	12.5000	1.2271	1.1077	-0.0000	11.2729	1.0000	11.2729	1
4	1	-3	231.3000	399.2133	-6.4919	-11.2739	32.0867	1.0000	32.0867	1
6	0	4	44.4000	20.2246	-2.2486	-3.8947	24.1754	1.0000	24.1754	1
6	2	4	32.0000	17.2503	-1.5961	-3.8344	14.7497	1.0000	14.7497	1
5	0	-4	380.2000	383.0317	-6.7645	11.7164	-2.8317	1.0000	-2.8317	1
4	2	-4	33.3000	21.6760	2.7004	-3.7924	11.6260	1.0000	11.6260	1
3	1	5	162.5000	160.0183	-9.5591	-8.8288	2.4859	1.0000	2.4859	1
3	0	-5	8.2000	19.6520	-2.2165	-3.8391	-11.4520	1.0000	-11.4520	1
2	2	6	85.9000	106.5043	10.3129	0.3856	-20.6043	1.0000	-20.6043	1
4	0	-6	110.5000	163.6337	11.9868	0.0000	-33.1837	1.0000	-33.1837	1
4	1	7	10.6000	12.7627	3.5617	-0.4681	-2.1627	1.0000	-2.1627	1
1	1	-7	78.0000	72.2755	-1.7725	-8.3147	5.7245	1.0000	5.7245	1
3	0	8	134.9000	132.1975	-5.7888	9.9573	2.7025	1.0000	2.7025	1
2	1	-8	37.2000	37.1470	6.0147	0.9850	0.0530	1.0000	0.0530	1
2	0	-9	10.8000	14.9334	3.8644	0.0000	-4.1334	1.0000	-4.1334	1

## AGREEMENT FACTORS BASED ON PARAMETERS BEFORE CYCLE 1

SUM(W\*(C-C)\*\*2) IS 0.2852E 05

SQR(T(SUM(W\*(C-C)\*\*2)/(N0-NV))) IS 39.8081

	NUMERATOR	DENOMINATOR	R
R FACTOR INCLUDING ZEROS	597.837	3095.200	0.193
R FACTOR OMITTING ZEROS	597.837	3095.200	0.193
WEIGHTED R FACTOR INCLUDING ZEROS	168.892	742.077	0.228
WEIGHTED R FACTOR OMITTING ZEROS	168.892	742.077	0.228

## EXAMPLE. HYPOTHETICAL PROBLEM BASED ON ALPHA QUARTZ.

## PARAMETERS AFTER LEAST SQUARES CYCLE 1

PARAMETER	OLD	CHANGE	NEW	ERROR
SCALE FACTOR	1.0000000	0.0005857	1.0005857	0.0064983
OVERALL B	0.		0.	
SI				
FORM FACTOR	1.0000000		1.0000000	
MULTIPLIER	1.0000000		1.0000000	
X	0.4100000	0.0053155	0.4153155	0.0006499
Y	0.2700000	-0.0023085	0.2676915	0.0008087
Z	0.1200000	-0.0025466	0.1174534	0.0006581
BETA(1,1)	0.0052482	-0.0026719	0.0025762	0.0023483
BETA(2,2)	0.0052482	-0.0019391	0.0033091	0.0022263
BETA(3,3)	0.0032528	-0.0005468	0.0027060	0.0007256
BETA(1,2)	0.0026241	-0.0028966	-0.0002725	0.0016950
BETA(1,3)	0.	-0.0009170	-0.0009170	0.0010200
BETA(2,3)	0.	0.0003482	0.0003482	0.0008362

## ESTIMATED AGREEMENT FACTORS BASED ON PARAMETERS AFTER CYCLE 1

SUM(W\*(O-C)\*\*2) IS 0.3070E 03  
 SQRTF(SUM(W\*(O-C)\*\*2)/(NG-NV)) IS 4.1300

## EXAMPLE. HYPOTHETICAL PROBLEM BASED ON ALPHA QUARTZ.

## CALCULATED Y BASED ON PARAMETERS BEFORE CYCLE 2

H	K	L	Y(OBS)	Y(CALC)	A	B	OBS-CALC	SIG(0)	(O-C)/SIG(0)	TQ
1	0	0	234.6000	232.7308	-15.2466	-0.0000	1.8692	1.0000	1.8692	1
1	1	0	317.5000	327.9457	-16.4159	-7.6210	-10.4457	1.0000	-10.4457	1
6	-1	0	76.0000	68.1950	-4.6793	-6.7985	7.8050	1.0000	7.8050	1
5	0	0	27.9000	23.2770	-1.9372	4.4155	4.6230	1.0000	4.6230	1
4	0	1	308.2000	312.7573	-6.8373	-15.3086	-4.5573	1.0000	-4.5573	1
3	1	1	56.5000	48.8201	-5.1902	4.6717	7.6799	1.0000	7.6799	1
3	2	1	1.5000	2.0536	-1.2360	-0.7236	-0.5586	1.0000	-0.5536	1
4	0	1	6.7000	3.3605	-1.7412	-0.5698	3.3395	1.0000	3.3395	1
3	-1	-1	199.8000	201.2066	-11.1717	-8.7272	-1.4066	1.0000	-1.4066	1
5	0	-1	145.8000	140.7784	-6.7253	9.7665	4.8215	1.0000	4.8215	1
2	0	2	78.7000	73.1369	4.2735	-7.4019	5.5631	1.0000	5.5631	1
6	1	2	11.5000	16.0669	2.7012	-2.9583	-4.5669	1.0000	-4.5669	1
5	0	2	38.0000	31.8800	1.7185	-5.6474	3.1200	1.0000	3.1200	1
3	0	-2	80.1000	84.4342	4.5917	7.0581	-4.3542	1.0000	-4.3342	1
5	-1	-2	45.2000	44.0862	-2.4543	6.1953	1.1138	1.0000	1.1138	1
3	0	-2	9.0000	13.2939	-2.0558	-3.0422	-4.2939	1.0000	-4.2939	1
3	0	-3	74.0000	75.0796	-8.6598	0.0000	-0.9796	1.0000	-0.9796	1
2	2	-3	212.0000	211.9543	14.4354	1.9239	0.0457	1.0000	0.0457	1
3	0	-5	12.5000	13.4910	3.6729	-0.0000	-0.9910	1.0000	-0.9910	1
4	-1	-3	231.3000	222.6463	-8.0450	-12.5565	8.6517	1.0000	8.6517	1
6	0	4	44.0000	45.3348	-3.3616	-5.8276	-0.9348	1.0000	-0.9348	1
6	2	4	32.0000	29.3684	-1.4792	-5.2102	2.6316	1.0000	2.6316	1
5	0	-4	180.2000	175.2345	-6.5199	11.2928	9.9655	1.0000	9.9655	1
4	2	-4	33.3000	28.9555	3.4983	-4.0846	4.3445	1.0000	4.3445	1
1	1	5	162.5000	162.6359	-9.2383	-8.7806	-0.4359	1.0000	-0.4359	1
3	0	-5	8.2000	7.8908	-1.4037	-2.4313	0.3092	1.0000	0.3092	1
2	2	6	85.9000	87.2194	9.3150	0.5905	-1.3194	1.0000	-1.3194	1
4	0	-6	110.5000	107.7016	10.3757	0.0000	2.7184	1.0000	2.7184	1
4	-1	7	10.6000	10.4373	3.1009	-0.8997	0.1627	1.0000	0.1627	1
1	1	-7	78.0000	75.4176	-1.8850	-8.4721	2.5824	1.0000	2.5824	1
3	0	8	134.9000	133.1443	-5.7660	9.9871	1.7557	1.0000	1.7557	1
2	1	-8	37.2000	35.5399	5.8589	1.0826	1.6601	1.0000	1.6601	1
2	0	-9	10.8000	12.6012	3.5477	0.0000	-1.8012	1.0000	-1.8012	1

## AGREEMENT FACTORS BASED ON PARAMETERS BEFORE CYCLE 2

SUM(W\*(O-C)\*\*2) IS 0.6391E 03

SQRTF(SUM(W\*(O-C)\*\*2)/(NC-NV)) IS 5.9588

	NUMERATOR	DENOMINATOR	R
R FACTOR INCLUDING ZEROS	111.083	3095.200	0.036
R FACTOR OMITTING ZEROS	111.083	3095.200	0.036
WEIGHTED R FACTOR INCLUDING ZEROS	25.281	742.077	0.034
WEIGHTED R FACTOR OMITTING ZEROS	25.281	742.077	0.034

EXAMPLE. HYPOTHETICAL PROBLEM BASED ON ALPHA QUARTZ.

PARAMETERS AFTER LEAST SQUARES CYCLE 2

PARAMETER	OLD	CHANGE	NEW	ERROR
SCALE FACTOR	1.0005857	-0.0002306	1.0003550	0.0030914
OVERALL S	0.		0.	
0				
FORM FACTOR	1.0000000		1.0000000	
MULTIPLIER	1.0000000		1.0000000	
X	0.4153155	0.0002572	0.4155727	C.0002937
Y	0.2676915	-0.000361	0.2676554	C.0003717
Z	0.1174534	0.0005464	0.1179998	C.0003146
BETA(1,1)	0.0025762	0.0013604	0.0039366	C.0009567
BETA(2,2)	0.0033E91	0.0012008	0.0045099	C.0009366
BETA(3,3)	0.0027C6E	0.000C222	0.0027282	C.0003574
BETA(1,2)	-0.0002725	0.0022977	0.0020252	C.0007473
BETA(1,3)	-0.000917E	0.0009445	0.0000276	C.0004045
BETA(2,3)	0.0003482	-0.0001149	0.0002333	C.0003995
SI				
FORM FACTOR	2.0000000		2.0000000	
MULTIPLIER	0.5000000		0.5000000	
X	0.5288597	0.0006168	0.5294765	C.0001849
Y	0.5288597		0.5288597	
Z	0.3333333		0.3333333	
BETA(1,1)	0.0092577	-0.0025950	0.0066626	C.0003353
BETA(2,2)	0.0092577		0.0092577	
BETA(3,3)	0.00411C8	-0.000C992	0.004C116	C.0001728
BETA(1,2)	0.0071120	-0.0036885	0.0034235	C.0005486
BETA(1,3)	0.0004649	-0.0002781	0.0001868	C.0001929
BETA(2,3)	-0.0004649		-0.0004649	

ESTIMATED AGREEMENT FACTORS BASED ON PARAMETERS AFTER CYCLE 2

SUM(W\*(O-C)\*\*2) IS 0.6423E C2  
 SQRTF(SUM(W\*(O-C)\*\*2)/(NC-NV)) IS 1.889E

EXAMPLE. HYPOTHETICAL PROBLEM BASED ON ALPHA QUARTZ.

CALCULATED Y BASED ON PARAMETERS BEFORE CYCLE 3

H	K	L	Y(OBS)	Y(CALC)	A	B	OBS-CALC	SIG(0)	(O-C)/SIG(0)	R
1	0	0	234.6000	234.4517	-15.2959	0.	0.4683	1.0000	0.4683	1
1	1	0	317.5000	317.0131	-16.2133	-7.3428	0.4869	1.0000	0.4869	1
6	1	0	76.0000	77.7327	-4.5320	-7.5590	-1.7327	1.0000	-1.7327	1
5	3	0	27.9000	28.2117	-1.5830	5.0681	-0.3117	1.0000	-0.3117	1
4	0	1	308.2000	308.9362	-8.7852	-15.2164	-0.7362	1.0000	-0.7362	1
3	1	1	56.5000	54.8334	-5.6606	4.7699	1.6666	1.0000	1.6666	1
3	2	1	1.5000	0.8846	-0.8137	-0.4710	0.1554	1.0000	0.1554	1
4	4	1	6.7000	5.3824	-2.2270	-0.6172	1.3176	1.0000	1.3176	1
3	1	-1	199.8000	199.6167	-11.0970	-8.7368	0.1833	1.0000	0.1833	1
5	2	-1	145.6000	147.9503	-8.8145	0.0702	-2.3503	1.0000	-2.3503	1
2	0	2	76.7000	76.9905	4.3857	-7.5962	1.7095	1.0000	1.7095	1
6	1	2	31.5000	31.3763	1.8161	-2.6591	1.1237	1.0000	1.1237	1
5	3	2	38.0000	37.2095	2.0457	-5.7144	0.7905	1.0000	0.7905	1
1	0	-2	80.4000	83.8707	4.5774	7.9283	-3.7707	1.0000	-3.7707	1
5	1	-2	45.2000	44.2917	-2.8921	5.9913	0.9083	1.0000	0.9083	1
3	2	-2	9.0000	9.9462	-1.3173	-2.8641	-0.9662	1.0000	-0.9662	1
3	0	3	74.1000	75.2471	-8.6714	0.0500	-1.1471	1.0000	-1.1471	1
2	2	3	212.0000	214.3139	14.4598	2.2528	-2.3139	1.0000	-2.3139	1
3	0	-3	12.5000	12.2621	3.5005	-8.0000	0.2379	1.0000	0.2379	1
4	1	-3	231.3000	231.6782	-8.0758	-12.8966	-0.3780	1.0000	-0.3780	1
6	0	6	44.4000	45.9496	-3.3861	-5.8684	-1.5496	1.0000	-1.5496	1
6	2	4	32.0000	30.1678	-1.3340	-5.3722	1.8322	1.0000	1.8322	1
5	0	-4	180.2000	180.1200	-6.7081	11.6187	0.0800	1.0000	0.0800	1
4	2	-4	53.3000	52.3981	3.8084	-4.2371	0.9019	1.0000	0.9019	1
1	1	5	162.5000	161.5392	-9.2103	-8.7519	0.9608	1.0000	0.9608	1
3	0	-5	8.2000	7.3109	-1.3515	-2.3408	0.8891	1.0000	0.8891	1
2	2	6	85.9000	86.7965	9.2960	0.5554	-0.8965	1.0000	-0.8965	1
4	0	-6	110.5000	109.9934	10.4843	0.0000	0.5066	1.0000	0.5066	1
4	3	7	10.0000	11.9148	3.3502	-0.8260	-1.3148	1.0000	-1.3148	1
1	3	-7	78.0000	75.7974	-1.6880	-8.5378	2.2026	1.0000	2.2026	1
3	0	8	134.9000	135.9982	-5.8288	10.0759	-1.0982	1.0000	-1.0982	1
2	3	-8	37.2000	37.1921	5.9645	1.2612	0.0079	1.0000	0.0079	1
2	0	-9	10.8000	12.8688	3.5860	0.0000	-2.0688	1.0000	-2.0688	1

AGREEMENT FACTORS BASED ON PARAMETERS BEFORE CYCLE 3

SUM(W\*(O-C)\*\*2) IS 0.63586 C2

SQRTF(SUM(W\*(O-C)\*\*2)/(NO-NV)) IS 1.8795

	NUMERATOR	DENOMINATOR	R
R FACTOR INCLUDING ZEROS	37.504	3095.200	0.012
R FACTOR OMITTING ZEROS	37.504	3095.200	0.012
WEIGHTED R FACTOR INCLUDING ZEROS	7.974	742.077	0.011
WEIGHTED R FACTOR OMITTING ZEROS	7.974	742.077	0.011

## EXAMPLE. HYPOTHETICAL PROBLEM BASED ON ALPHA QUARTZ.

## CORRELATION MATRIX

1	1.0000	-0.2333	-0.4564	0.3507	0.3961	0.1185	0.1093	0.2206	0.3141	-0.0880
2	0.	1.0000	0.6823	-0.3275	-0.1397	0.2778	-0.0905	0.3230	-0.2742	-0.0365
3	0.	0.	1.0000	-0.4928	0.0294	0.0029	-0.0474	0.2678	-0.3861	-0.1187
4	0.	0.	0.	1.0000	-0.2308	-0.0646	0.2524	-0.3875	0.5313	0.1682
5	0.	0.	0.	0.	1.0000	-0.3491	-0.1624	0.4986	0.0317	-0.3117
6	0.	0.	0.	0.	0.	1.0000	-0.1114	0.4683	-0.1232	0.2852
7	0.	0.	0.	0.	0.	0.	1.0000	-0.1634	0.1426	0.0746
8	0.	0.	0.	0.	0.	0.	0.	1.0000	-0.1179	-0.0091
9	0.	0.	0.	0.	0.	0.	0.	0.	1.0000	0.1294
10	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0000
11	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
12	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
13	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
14	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
15	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.



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